Fractional and irrational differential systems: approximation and optimization

T. HÉLIE

Collaboration with D.Matignon and R. Mignot

Fractional Derivatives for Mechanical Engineering - State-of-the-art and
 Applications —

- 1 Introduction : zoology and basic ideas
- Systems under consideration
 - Integral representations with poles and cuts
 - Finite-dimensional approximation by interpolation
- Specialized optimization procedures
 - Functional spaces and measures
 - Regularized criterion with equality constraints
 - Numerical optimization
- 4 Applications
 - Fractional systems
 - Irrational systems
- Conclusion and Perspectives

Outline

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Zoology of Contractional (/Irrational) Syst.

Fractional/Irrational syst.	Transfer fct. (analytic in $\Re e(s) > 0$)
Integrator I _{1/2}	$H_1(s) = 1/\sqrt{s} \ (\to H(s)^2 = 1/s)$
Derivative $\partial_t^{1/2}$	$H_2(s) = \sqrt{s} \ (\rightarrow H(s)^2 = s)$
Frac. Diff. Eq. $(0 < \alpha < 1)$	$H_3(s) = \sum_{q=0}^{Q} s^{q\alpha} / \sum_{p=0}^{P} s^{p\alpha}$
$\sum_{p=0}^{P} \partial_t^{p\alpha} \mathbf{y} = \sum_{q=0}^{Q} \partial_t^{q\alpha} \mathbf{e}$	$ 13(3) - \angle_{q=0} 3 \cdot / \angle_{p=0} 3$

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	$H_4(s) = 1/\sqrt{s^2 + 1}$
Fract. PDE : $(\partial_z + \partial_t^{1/2})x = 0$ $y(t) = x(z, t), \partial_z x(0, t) = -e(t)$	$H_5(s) = e^{-\sqrt{s}z}/\sqrt{s}$
Flared lossy acoustic pipe	$H_6(s) = 2\Gamma(s)e^{s-\Gamma(s)}/[s+\Gamma(s)]$ with $\Gamma(s) = \sqrt{s^2 + \varepsilon s^{3/2} + 1}$

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- \rightarrow singularities of $H_k(s)$: poles and cuts in $\Re e(s) < 0$



Appl

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 \mathbb{R}^- is called a cut of $H_1(s)$ and the jump at $-\xi \in \mathbb{R}^-$ is

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- Why choosing the cut \mathbb{R}^- (that is $\theta \in]-\pi,\pi]$) ?
 - (i) Causal stable system $\Rightarrow H$ analytic in $\Re e(s) > 0$
 - (ii) It is "natural" to preserve the Hermitian symmetry since a real system $\Rightarrow H_1(\overline{s}) = \overline{H_1(s)}$ in $\Re e(s) > 0$

Let $e_+^t = e^t \mathbf{1}_{\mathbb{R}^+}(t)$ be the causal exponential.

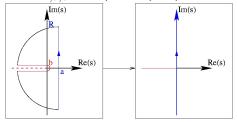
• Causal convolution kernel :
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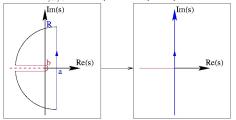
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- Bromwich contour $C_{R,a,b}$ with $(R,a,b) \rightarrow (+\infty,0^+,0^+)$



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$$h(t) + 0 - \int_0^{+\infty} \mu(-\xi) e_+^{-\xi t} d\xi + 0 = 0$$
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- Time-realization : $\begin{cases} \partial_t \phi(-\xi,t) = -\xi \phi(-\xi,t) + e(t), & \phi(-\xi,0) = 0, \quad \forall \xi > 0 \\ y(t) = \int_0^{+\infty} \mu(-\xi)\phi(-\xi,t) d\xi \end{cases}$
- Transfer function : aggregation of first order systems $F(-\xi,s) = \frac{\Phi(-\xi,s)}{E(s)} = \frac{1}{s+\xi}, \quad \forall \xi > 0$ $H_1(s) = \frac{Y(s)}{E(s)} = \frac{\int_0^{+\infty} \mu(-\xi)\Phi(-\xi,s)d\xi}{E(s)} = \int_0^{+\infty} \mu(-\xi)F(-\xi,s)d\xi$ $= \int_0^{+\infty} \frac{\mu(-\xi)}{s+\xi}d\xi \left(= \frac{1}{\sqrt{s}} \right), \quad \text{for } \Re e(s) > 0$

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- Are such integral representations always well-posed?
- How to perform accurate approximations and simulations in the time domain?



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Definitions

• Many transfer functions can be decomposed as follows, in some right-half complex plane $\mathbb{C}_a^+ := \{\Re e(s) > a\}$,

$$H(s) = \sum_{k=1}^{K} \sum_{l=1}^{L_k} \frac{r_{k,l}}{(s - s_k)^l} + \int_{\mathcal{C}} \frac{M(d\gamma)}{s - \gamma},$$

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 which translates in the time domain into the following decomposition of the impulse response:

$$h(t) = \sum_{k=1}^{K} \sum_{l=1}^{L_k} r_{k,l} \frac{1}{l!} t^{l-1} e^{s_k t} + \int_{\mathcal{C}} e^{\gamma t} M(d\gamma), \quad \text{for } t > 0.$$

Appl

Integral representations with poles and cuts

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• The integral part can be realized by a dynamical system:

$$\partial_t \phi(\gamma, t) = \gamma \phi(\gamma, t) + u(t), \quad \phi(\gamma, 0) = 0, \qquad \forall \gamma \in \mathcal{C}$$

$$y(t) = \int_{\mathcal{C}} \phi(\gamma, t) M(d\gamma),$$

Some technical conditions

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• When measure M has a density μ , and the curve \mathcal{C} admits a \mathcal{C}^1 -regular parametrization $\xi \mapsto \gamma(\xi)$ which is non-degenerate $(\gamma'(\xi) \neq 0)$, we have :

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Note the hermitian symmetry property :

$$H(s) = \overline{H(\overline{s})}, \, \forall s \in \mathbb{C}_a^+$$

Approximation by interpolation of the state

• Approximation of the state $\phi(\gamma, t)$, for $\{\gamma_p\}_{0 \le p \le P+1} \subset \mathcal{C}$ $\widetilde{\phi}(\gamma, t) = \sum_{p=1}^{P} \phi_p(t) \Lambda_p(\gamma)$, where $\phi_p(t) = \phi(\gamma_p, t)$.

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- The corresponding realization reads :

$$\begin{split} \partial_t \phi_{p}(t) &= \gamma_p \, \phi_{p}(t) + u(t), \, 1 \leq p \leq P, \\ \widetilde{y}(t) &= \Re \sum_{p=1}^P \mu_p \, \phi_{p}(t) \quad \text{with } \mu_p = \int_{[\gamma_{p-1}, \gamma_{p+1}]_{\mathcal{C}}} \mu(\gamma) \Lambda_p(\gamma) \mathrm{d}\gamma. \end{split}$$

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$$\widetilde{H}_{\mu}(s) = \frac{1}{2} \sum_{p=1}^{P} \left[\frac{\mu_p}{s - \gamma_p} + \frac{\overline{\mu_p}}{s - \overline{\gamma_p}} \right]$$

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Convergence results can be proved, as dim. P → ∞.



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Norms in L², or Sobolev spaces H^s, are defined as :

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, with $w_{\mathbf{S}}(f) = (1+4\pi^2 f^2)^{\mathbf{S}}$.

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 For specific applications, more general frequency dependent weights can be used: bounded frequency range, logarithmic scale, relative error measurement, bounded dynamics... For audio applications, w(f) can be adapted and modified according to the following requirements :

1 a bounded frequency range $f \in [f^-, f^+] : w(f) \mathbf{1}_{[f^-, f^+]}(f)$;

Building up specific weights for audio applications

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- 2 a frequency log-scale : w(f)/f;

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- **1** a bounded frequency range $f \in [f^-, f^+]$: $w(f) \mathbf{1}_{[f^-, f^+]}(f)$;
- 2 a frequency log-scale : w(f)/f;
- **3** a relative error measurement : $w(f)/|H(2i\pi f)|^2$

Building up specific weights for audio applications

For audio applications, w(f) can be adapted and modified according to the following requirements :

- **1** a bounded frequency range $f \in [f^-, f^+]$: $w(f) \mathbf{1}_{[f^-, f^+]}(f)$;
- 2 a frequency log-scale : w(f)/f;
- **3** a relative error measurement : $w(f)/|H(2i\pi f)|^2$
- **3** a relative error on a bounded dynamics : $w(f)/(\operatorname{Sat}_{H,\Theta}(f))^2$ where the saturation function $\operatorname{Sat}_{H,\Theta}$ with threshold Θ is defined by

$$\mathsf{Sat}_{H,\Theta}(f) = \left\{ egin{array}{ll} |H(2i\pi f)| & \mathsf{if} \ |H(2i\pi f)| \geq \Theta_H \ \Theta_H & \mathsf{otherwise} \end{array}
ight.$$

Note: normalization of the samples is desirable in most audio applications, before the sequence is sent to DAC audio converters.



• The regularized criterion reads :

$$C_{R}(\mu) = \int_{\mathbb{R}^{+}} \left| \widetilde{H_{\mu}}(2i\pi f) - H(2i\pi f) \right|^{2} w(f) df + \sum_{p=1}^{P} \epsilon_{p} |\mu_{p}|^{2},$$

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• Equality constraints for $\widetilde{H_{\mu}}^{(d_j)}$ at prescribed frequency points η_j , $1 \le j \le J$ are taken into account thanks to a Lagrangian $\mathcal{C}_{R,L}$ by adding to \mathcal{C}_R :

$$\Re e \left(\ell^* \left[egin{array}{c} H^{(d_1)}(2i\pi\eta_1) - \widetilde{H_{\mu}}^{(d_1)}(2i\pi\eta_1) \ dots \ H^{(d_J)}(2i\pi\eta_J) - \widetilde{H_{\mu}}^{(d_J)}(2i\pi\eta_J) \end{array}
ight]
ight),$$

Discrete criterion

• Discrete version of the criterion for frequencies increasing from $f_1 = f_-$ to $f_{N+1} = f_+$ is, with $s_n = 2i\pi f_n$:

$$\mathcal{C}(\mu) \approx \sum_{n=1}^{N} w_n \left| \widetilde{H_{\mu}}(s_n) - H(s_n) \right|^2 \text{ with } w_n = \int_{f_n}^{f_{n+1}} w(f) df.$$

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In matrix notations, this rewrites

$$\mathcal{C}_{\mathsf{R},\mathsf{L}}(\mu) = ig(\mathbf{M} \mu \! - \! \mathbf{h} ig)^* \mathbf{W} ig(\mathbf{M} \mu \! - \! \mathbf{h} ig) \! + \! \mu^t \mathbf{E} \mu \! + \! \Re ig(\ell^* \left[\mathbf{k} - \mathbf{N} \mu
ight] ig),$$

$$\text{with} \left\{ \begin{array}{ll} \textbf{\textit{M}}: & \text{model} & \textbf{\textit{N}} \times (P + P_2) \\ \textbf{\textit{N}}: & \text{constraint model} & \textbf{\textit{J}} \times (P + P_2) \\ \textbf{\textit{E}}: & \text{regularization} & (P + P_2) \times (P + P_2) \\ \textbf{\textit{W}}: & \text{weights} & \textbf{\textit{N}} \times \textbf{\textit{N}} \\ \textbf{\textit{h}}: & \text{data} & \textbf{\textit{N}} \times \textbf{\textit{1}} \\ \textbf{\textit{k}}: & \text{constaints} & \textbf{\textit{J}} \times \textbf{\textit{1}} \end{array} \right.$$

Closed-form solution

• If J = 0 (no constraint), the solution reduces to

$$\mu = \mathcal{M}^{-1}\mathcal{H}$$
,

where
$$\mathcal{M} = \Re e \left(\mathbf{M}^* \mathbf{W} \mathbf{M} + \mathbf{E} \right)$$
 and $\mathcal{H} = \Re e \left(\mathbf{M}^* \mathbf{W} \mathbf{h} \right)$.

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• For $J \ge 1$, the solution reads :

$$\mu = \mathcal{M}^{-1} \left[\mathcal{H} + \underline{\mathbf{N}}^t \mathcal{N}^{-1} \left(\underline{\mathbf{k}} - \underline{\mathbf{N}} \mathcal{M}^{-1} \mathcal{H} \right) \right],$$

where $\mathcal{N} = \underline{\mathbf{N}} \mathcal{M}^{-1} \underline{\mathbf{N}}^t$ is invertible for non-redundant constraints, and $\left\{ \begin{array}{ll} \underline{\mathbf{N}}^t & \text{denotes} & [\Re(\mathbf{N}^t), \Im(\mathbf{N}^t)] \\ \underline{\mathbf{k}}^t & \text{denotes} & [\Re(\mathbf{k}^t), \Im(\mathbf{k}^t)] \end{array} \right.$.

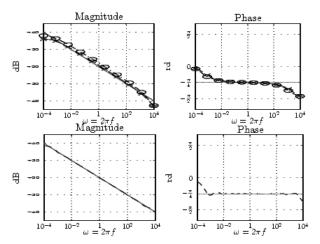
Outline

- Introduction: zoology and basic ideas
- Systems under consideration
 - Integral representations with poles and cuts
 - Finite-dimensional approximation by interpolation
- Specialized optimization procedures
 - Functional spaces and measures
 - Regularized criterion with equality constraints
 - Numerical optimization
- Applications
 - Fractional systems
 - Irrational systems
- Conclusion and Perspectives



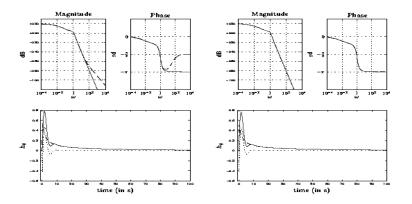
An academic example:

$$H_1(s) = 1/\sqrt{s}, \ \mu_1(-\xi) = 1/(\pi\sqrt{\xi})$$



Top: Interpolation, P = 16. Bottom: Optimization, P = 10.



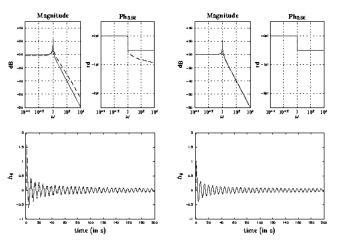


Left: Interpolation, P = 18. Right: Optimization, P = 18! (...): poles only. (--): cut only. (-): poles and cut.



Appl

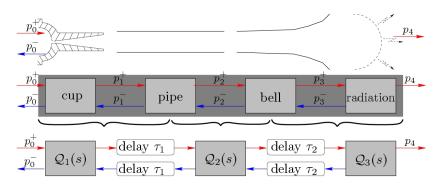
$$H_4(s) = 1/\sqrt{s^2 + 1}, \;\; \mu_4^{\pm}(-\xi) = 1/(\pi\sqrt{\xi(\pm 2i - \xi)})$$



Left: Interpolation, P = 10. Right: Optimization, P = 10!



Decomposition into elementary subsystems.



Transfer functions of interest:

- Reflection between p_0^+ and p_0^- .
- Transmission between p_0^+ and p_4 .

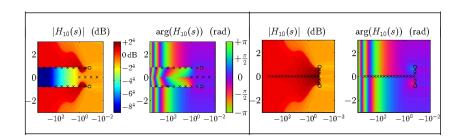


Appl

Trumpet-like instrument (II): various choices of the cuts

with 3 Horizontal cuts,

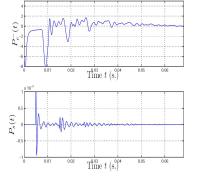
with a Cross cut



• Remark : the values of H(s) in \mathbb{C}_0^+ do not depend on the choice of the cut!

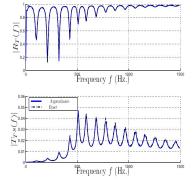


Time-domain representation



Frequency-domain rep.

Appl



Real-time simulations in Pure-Data environment on optimized models with $P \le 10$ for each quadripole Q_k : bounded freq. range, log-scale & relat. error.

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Perspectives

• Open question : choice of the cut?

Perspectives

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- Open question : optimal placement of the poles, once the cut has been chosen?

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- Open question : choice of the cut?
- Open question : optimal placement of the poles, once the cut has been chosen?
- What can not be represented by poles and cuts?
 - Delay systems stemming from wave propagation phenomena.
 - systems of PDEs with variable coefficients: must be decomposed into subsystems with constant coefficients.

Conclusion

A powerful and very flexible method of simulation of some infinite-dimensional linear systems has been presented: it uses a simple optimization procedure with parameters which are meaningful from a signal processing point of view, and it enables a low cost simulation (both in the frequency domain and in the time domain), even suitable for real-time applications.

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- From a a theoretical point of view, this method is based on a representation with poles and cuts, which generalizes the so-called diffusive representations.
- Many such systems, among which fractional differential systems, have been presented here and elsewhere, which clearly illustrates the generality, the flexibility and the power of this method.

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