

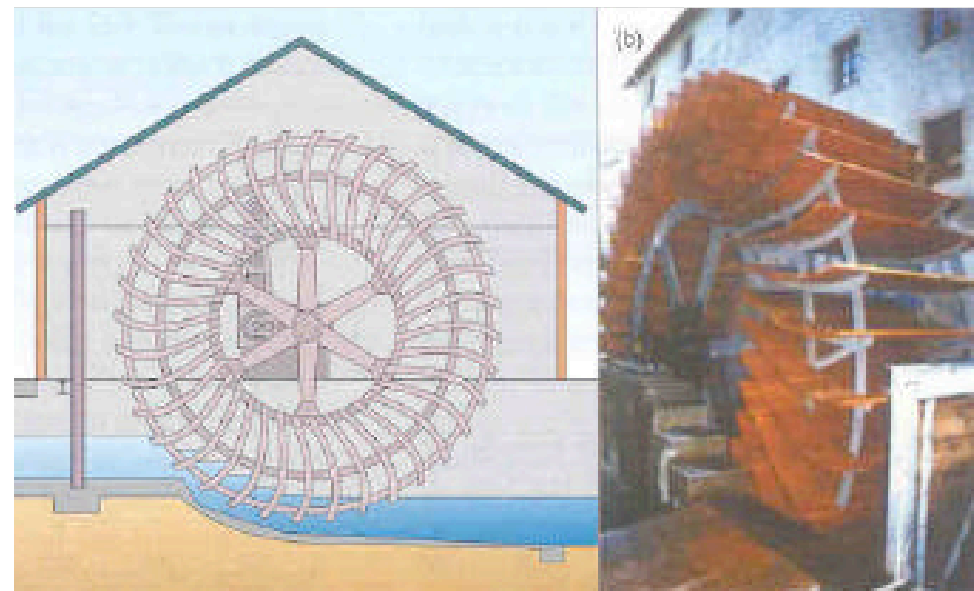
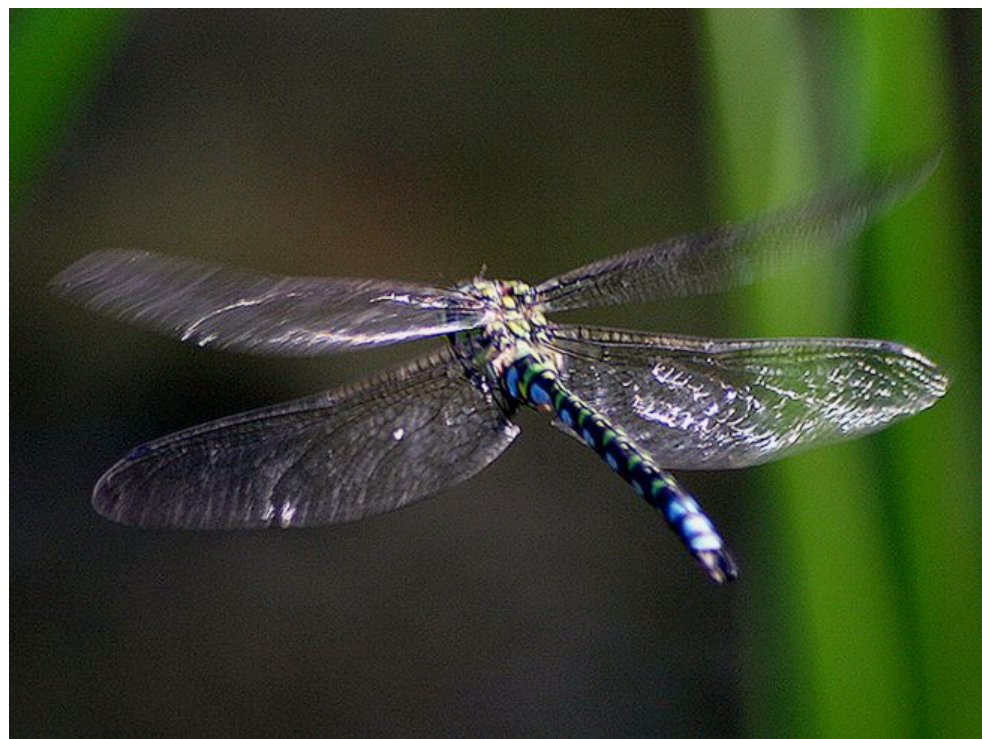
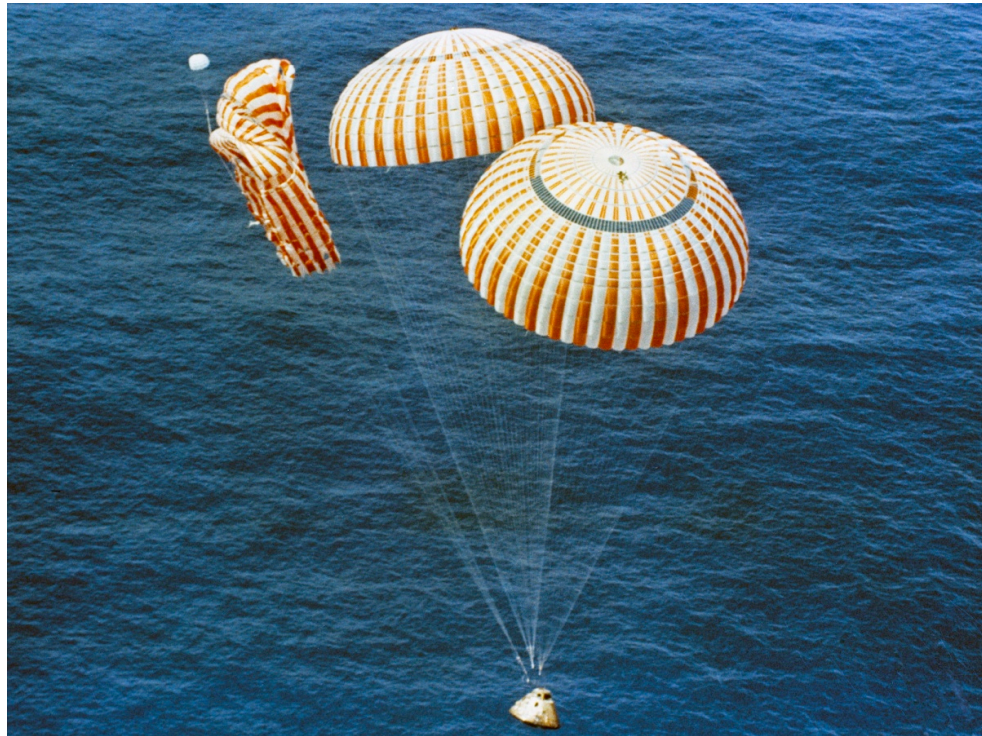
Enriched Space-Time FEM Method for Large Motion of Thin Flexible Structures Immersed in a Fluid

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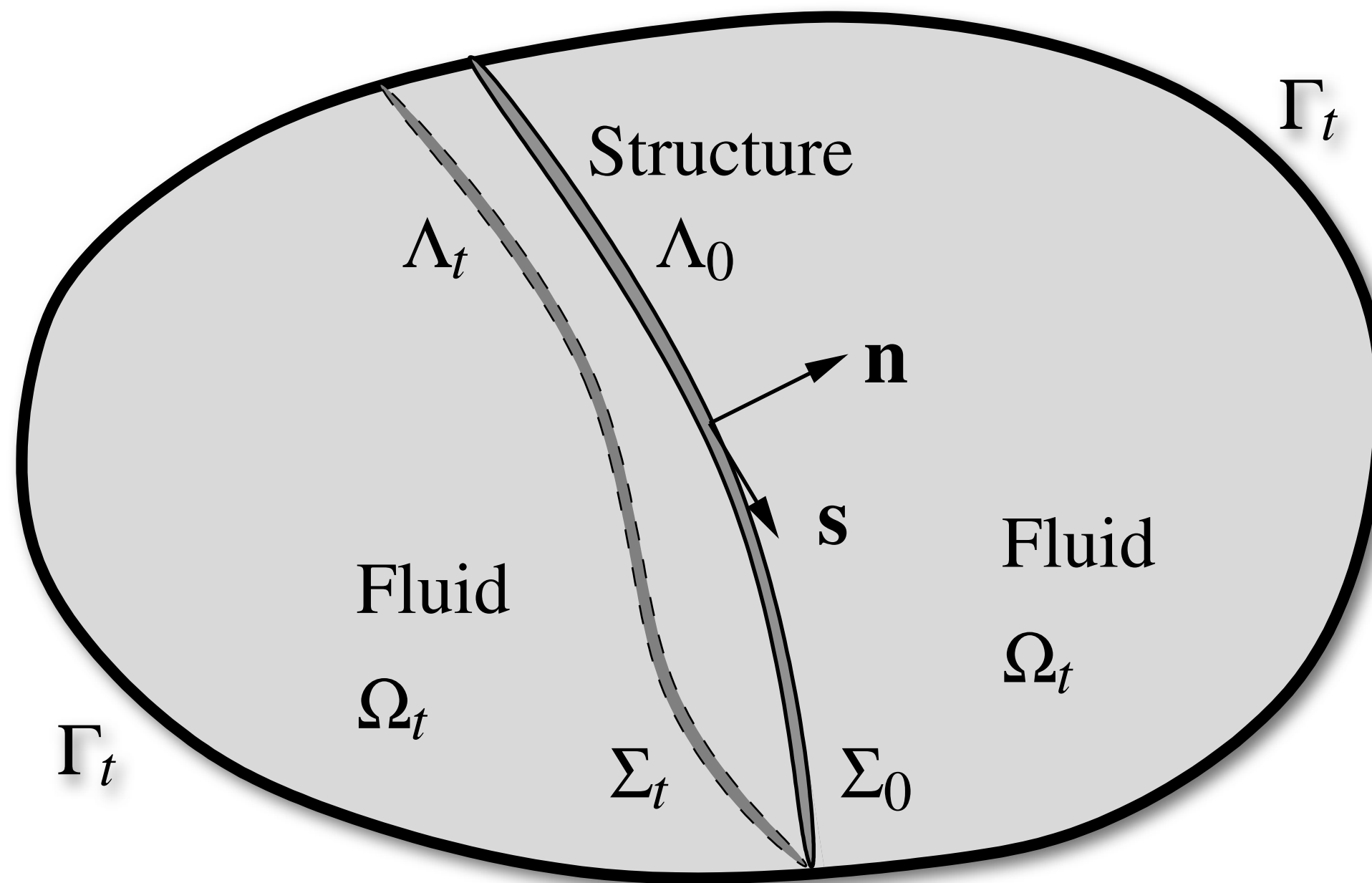
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Interaction of Flow and Structure



The Surface Coupled Problem

- flexible thin-walled structure immersed in viscous fluid flow
- large translations, rotations and deformations of the thin structure



Governing Equations: Strong Form

Fluid: incompressible, Newtonian, velocity-pressure based

$$\rho \mathbf{v}_{,t} + \rho \mathbf{v} \cdot \nabla \mathbf{v} - \nabla \cdot \mathbf{T} - \rho \mathbf{b} = \mathbf{0} \quad \text{in } Q_t$$

$$\nabla \cdot \mathbf{v} = 0 \quad \text{in } Q_t$$

$$\mathbf{T} = -p\mathbf{I} + 2\mu\mathbf{D} \quad \text{in } Q_t$$

$$\mathbf{D} = \frac{1}{2}(\nabla \mathbf{v} + (\nabla \mathbf{v})^T) \quad \text{in } Q_t.$$

Structure: thin-walled, large deformations/strains, velocity-stress based

$$\mathbf{w} = [v_X \quad v_Y \quad \omega]^T$$

$$\mathbf{s} = [N \quad Q \quad M]^T$$

$$\rho \mathbf{G} \dot{\mathbf{w}} - (\mathbf{F}\mathbf{s})_{,X} - (\mathbf{H}\mathbf{s}) - \rho \mathbf{G}\mathbf{b} = \mathbf{0} \quad \text{in } L_0$$

$$\mathbf{C}^{-1} \dot{\mathbf{s}} - \dot{\mathbf{e}} = \mathbf{0} \quad \text{in } L_0.$$

Interface Conditions: velocity-traction based

$$\mathbf{v}^F - \mathbf{v}^S = \mathbf{0} \quad \text{on } R_t$$

$$\mathbf{t}^F + \frac{d\Sigma_0}{d\Sigma_t} \mathbf{t}^S = \mathbf{0} \quad \text{on } R_t$$

Governing Equations: Weak Form

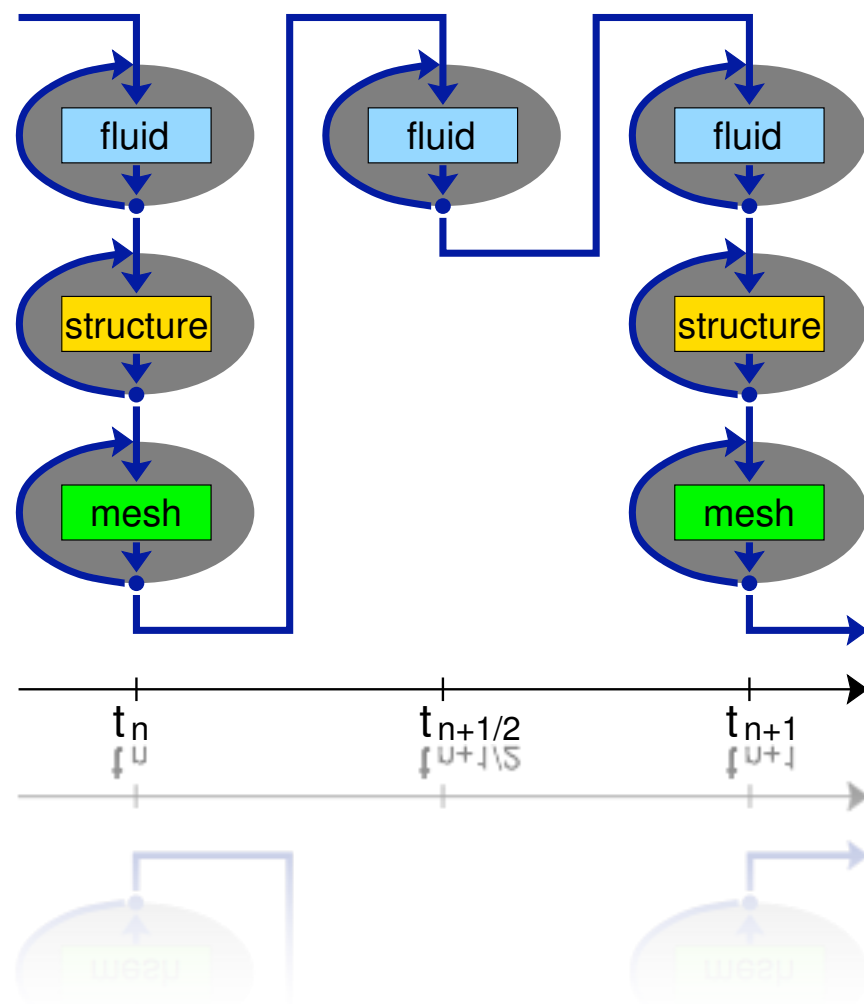
- Weighted residual method on the space-time domain
- Lagrange multiplier technique for coupling conditions

$$\begin{aligned}
 & \int_{Q_t^n} \delta \mathbf{v} \cdot \rho (\mathbf{v}_{,t} + \mathbf{v} \cdot \nabla \mathbf{v}) dQ_t + \int_{Q_t^n} \delta \mathbf{D} : 2\mu \mathbf{D} dQ_t - \int_{Q_t^n} \nabla \cdot (\delta \mathbf{v}) p dQ_t - \int_{Q_t^n} \delta \mathbf{v} \cdot \rho \mathbf{b} dQ_t \\
 & + \int_{Q_t^n} \delta p \nabla \cdot \mathbf{v} dQ_t \\
 & - \int_{P_t^{n,g}} \delta \mathbf{v} \cdot \mathbf{t} dP_t + \int_{P_t^{n,g}} \delta \mathbf{t} \cdot (\mathbf{v} - \bar{\mathbf{v}}) dP_t - \int_{P_t^{n,h}} \delta \mathbf{v} \cdot \bar{\mathbf{t}} dP_t \\
 & + \int_{\Omega_t^n} \delta \mathbf{v}(t_n^+) \cdot \rho (\mathbf{v}(t_n^+) - \mathbf{v}(t_n^-)) d\Omega_t \\
 & + \sum_e \int_{Q_t^n} (\rho \delta \mathbf{v}_{,t} + \rho \mathbf{v} \cdot \nabla (\delta \mathbf{v}) - \nabla \cdot (\delta \mathbf{T})) \cdot \tau_m \frac{1}{\rho} (\rho \mathbf{v}_{,t} + \rho \mathbf{v} \cdot \nabla \mathbf{v} - \nabla \cdot \mathbf{T} - \rho \mathbf{b}) dQ_t \\
 & + \sum_e \int_{Q_t^n} \nabla \cdot (\delta \mathbf{v}) \cdot \tau_c \rho \nabla \cdot \mathbf{v} dQ_t = 0 \quad \forall \delta \mathbf{v}, \delta p, \delta \mathbf{t}.
 \end{aligned}$$

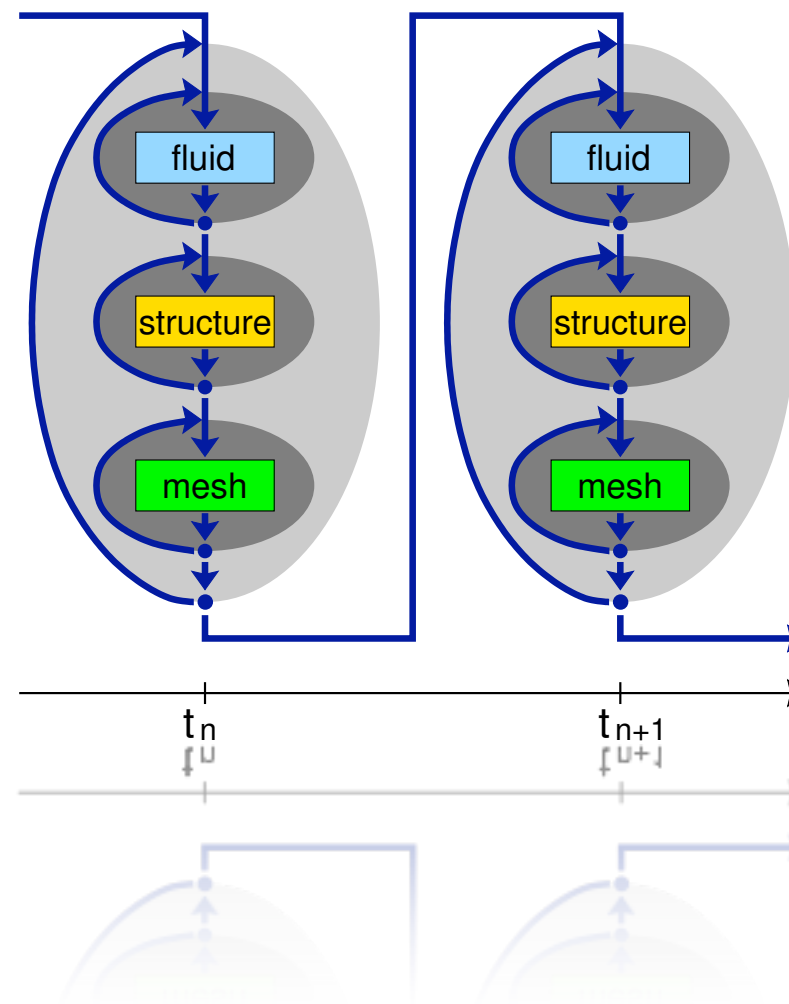
$$\begin{aligned}
 & \int_{L_0^n} \delta \mathbf{w} \cdot \rho \mathbf{G} \dot{\mathbf{w}} dX + \int_{L_0^n} \delta \dot{\mathbf{e}} \cdot \mathbf{s} dX - \int_{L_0^n} \delta \mathbf{w} \cdot \rho \mathbf{G} \mathbf{b} dX \\
 & + \sum_e \int_{L_0^n} \delta \mathbf{s} \cdot (\mathbf{C}^{-1} \dot{\mathbf{s}} - \dot{\mathbf{e}}) dX \\
 & - [\delta \mathbf{w} \cdot \bar{\mathbf{s}}]_{\bar{P}_0^{n,h}} \\
 & - \int_{\bar{P}_0^{n,h}} \delta \mathbf{w} \cdot \bar{\mathbf{t}} dX \\
 & + \int_{L_0^n} \delta \mathbf{w}(t_n^+) \cdot \rho \mathbf{G} (\mathbf{w}(t_n^+) - \mathbf{w}(t_n^-)) dX \\
 & + \int_{L_0^n} \delta \mathbf{s}(t_n^+) \cdot \mathbf{C}^{-1} (\mathbf{s}(t_n^+) - \mathbf{s}(t_n^-)) dX = 0 \quad \forall \delta \mathbf{w}, \delta \mathbf{s}.
 \end{aligned}$$

$$+ \int_{R_t^n} \delta \mathbf{t}^F \cdot (\mathbf{v}^F - \mathbf{v}^S) dR - \int_{R_t^n} \delta \mathbf{v}^F \cdot \mathbf{t}^F dR + \int_{R_t^n} \delta \mathbf{v}^S \cdot \mathbf{t}^F dR$$

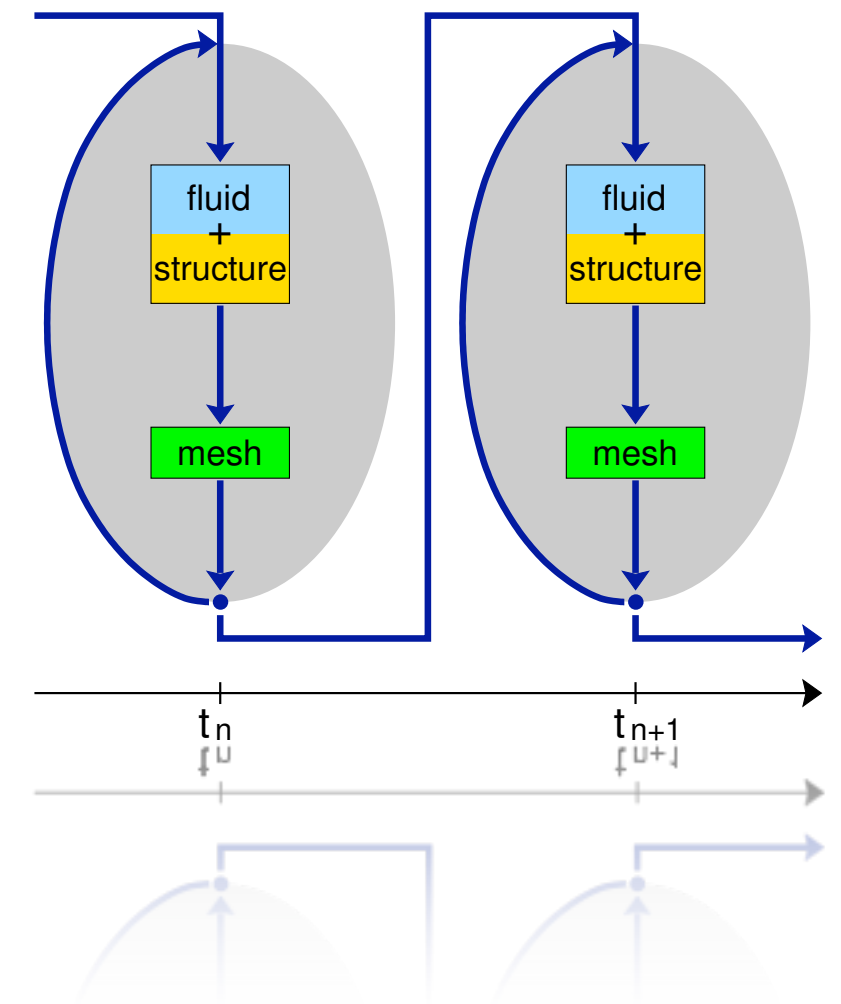
Coupling Schemes



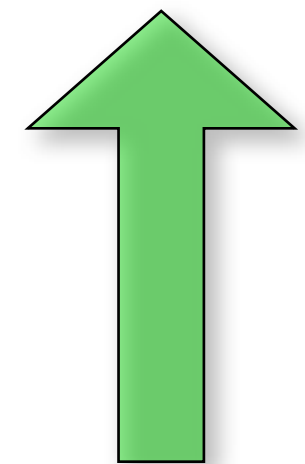
weak coupling



strong coupling
(partitioned)

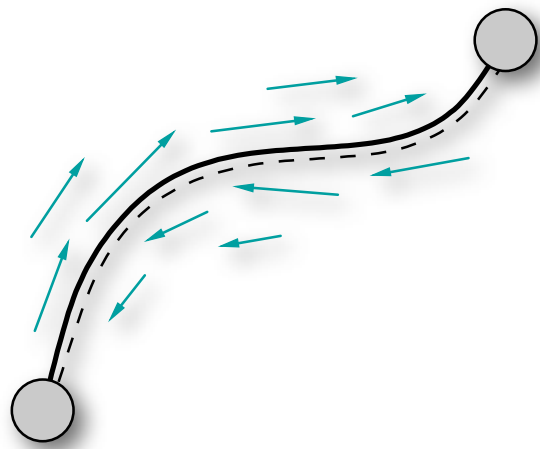


strong coupling
(monolithic, simultaneous)

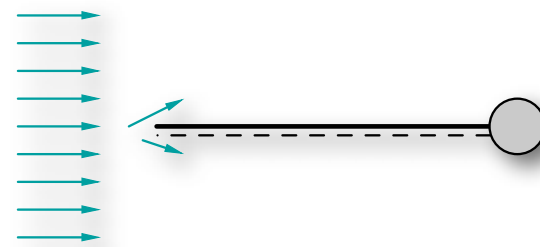


Appearance of Non-smooth Fluid Solutions

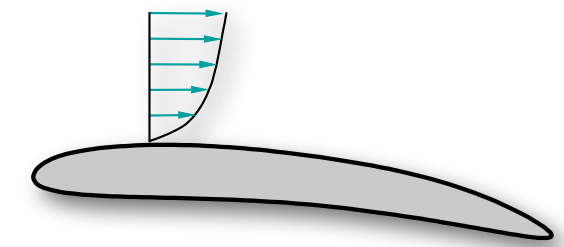
- flow-immersed thin structures cause discontinuous flow solutions !



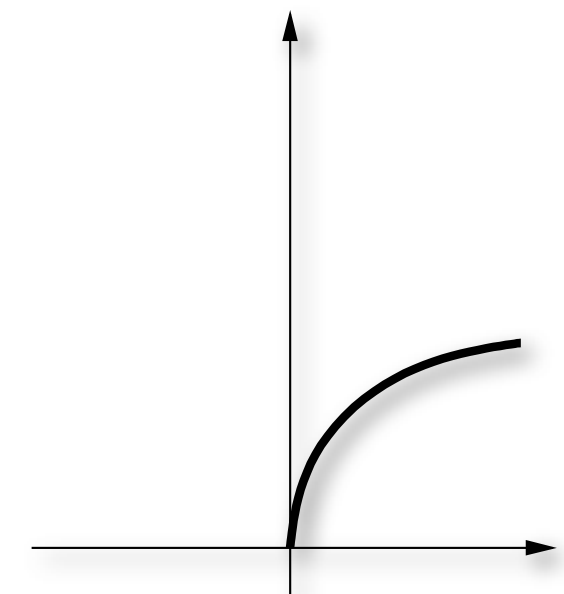
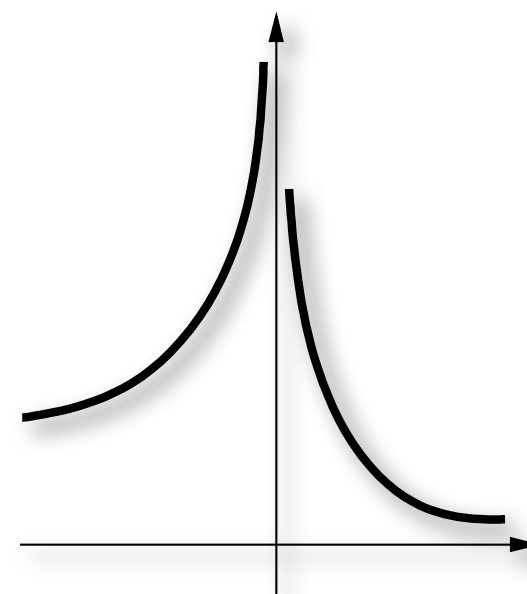
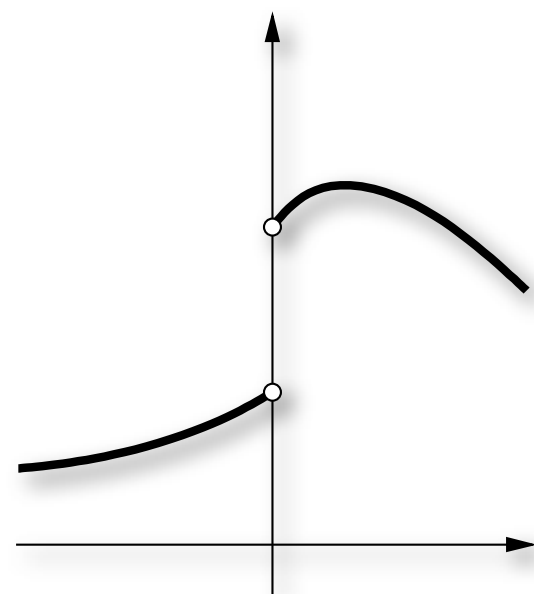
Navier-Stokes fluid (v-p) & slip interface conditions



Navier-Stokes fluid (v-p) & tip singularity



Navier-Stokes fluid (v-p) & shear layer at interface

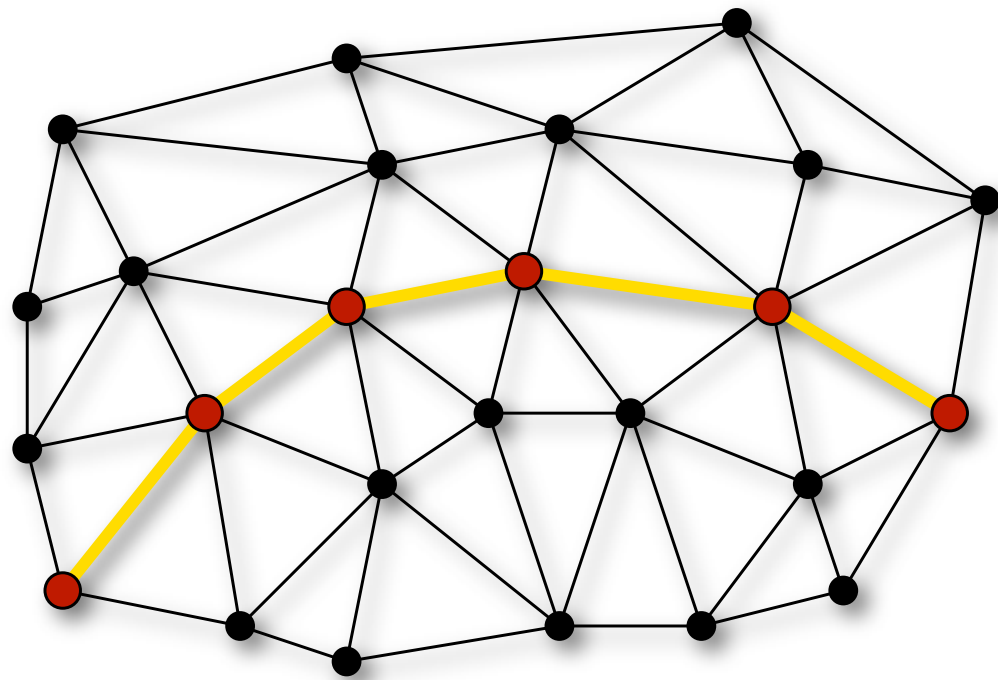


no-slip interface

- strongly discontinuous pressure
- weakly discontinuous velocity

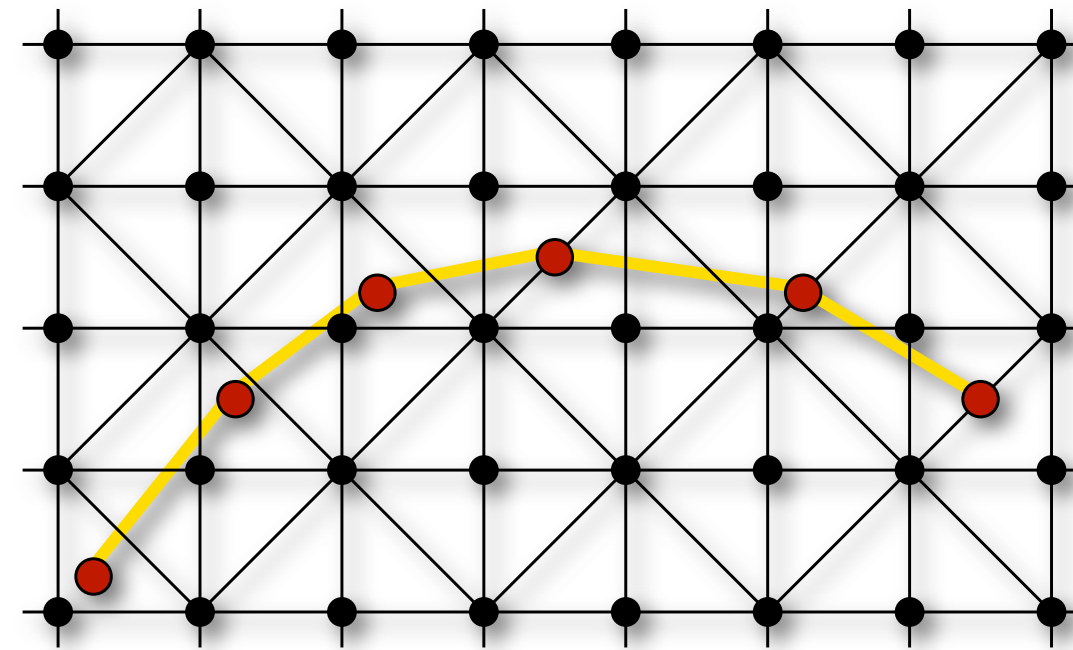
Approximation of Non-smooth Solutions

- Explicit Methods

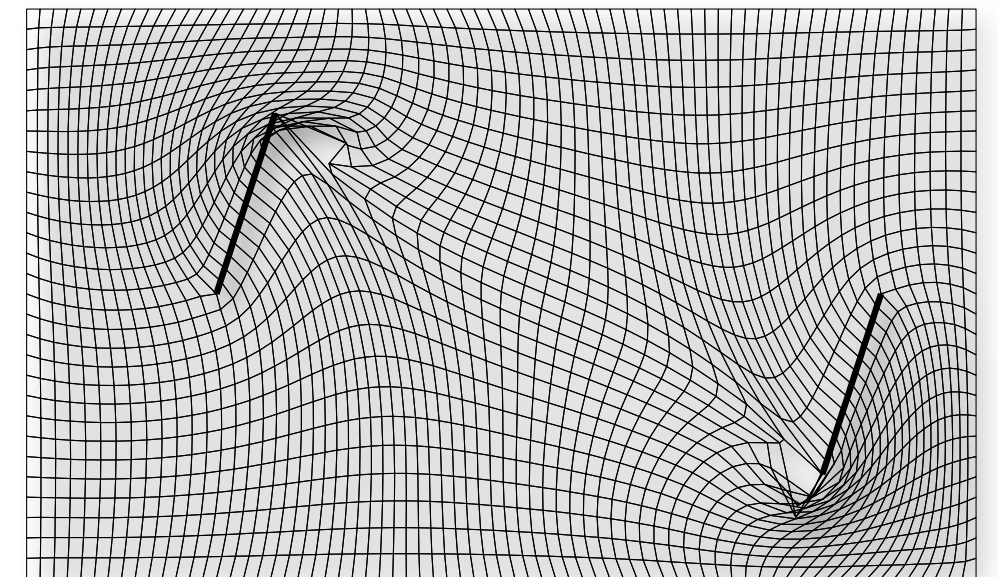
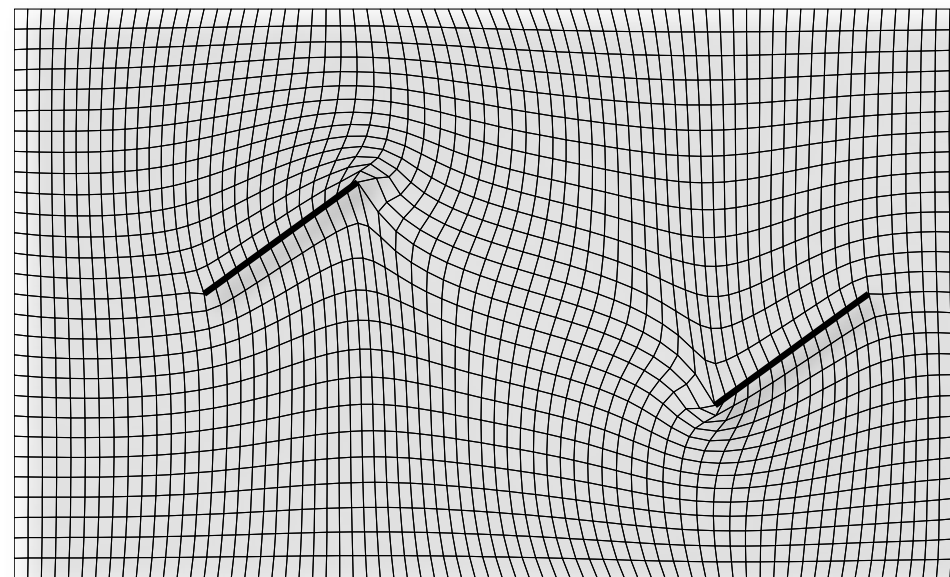
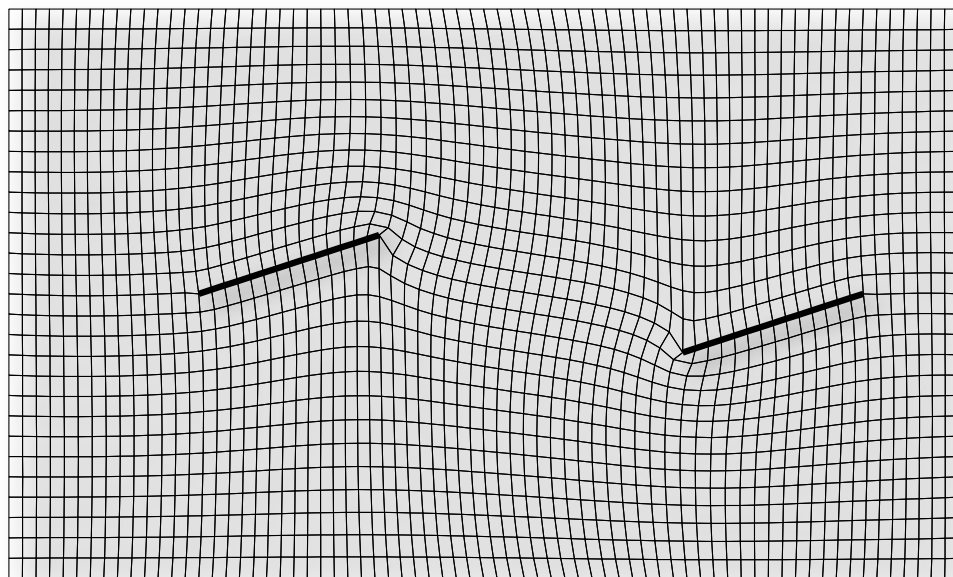


- fixed connectivity
- mesh moving / remeshing

- Implicit Methods

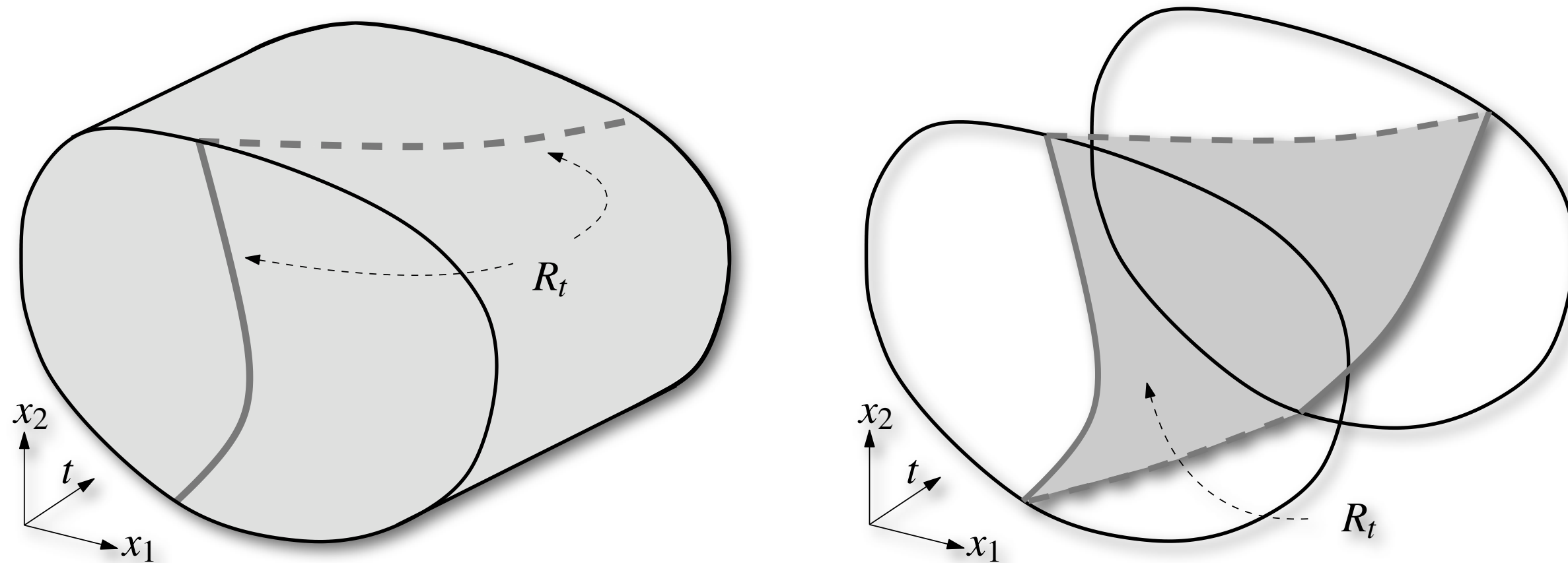


- changing connectivity
- update of indicator function



Evolving Non-smooth Solutions

- The stated problem involves discontinuities at moving interfaces

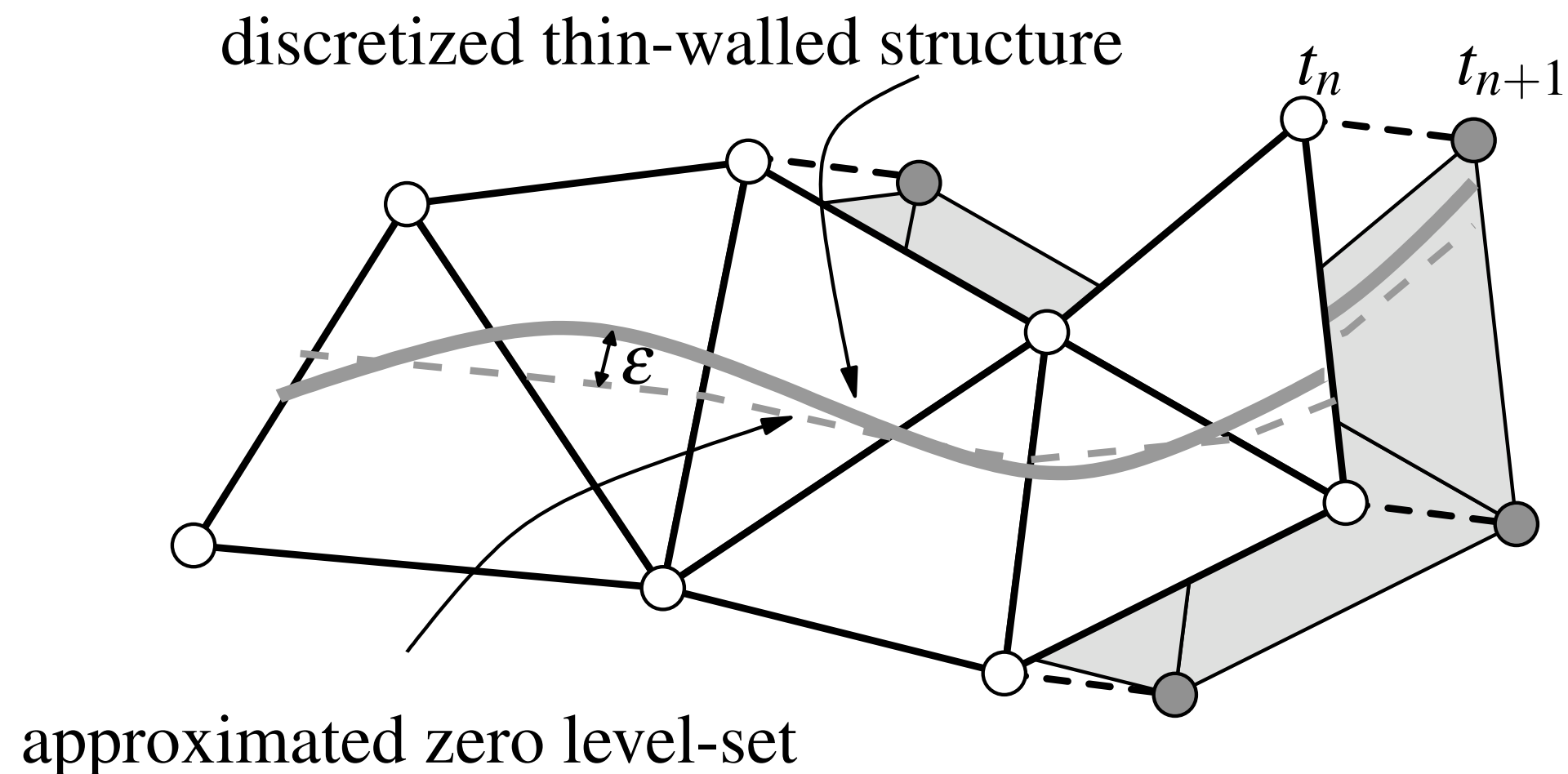


- ▶ Localization of non-smooth solution by implicit function (Level Sets)
- ▶ Incorporation of a priori knowledge on solution characteristics (XFEM)

Level Set Representation of Thin Structure

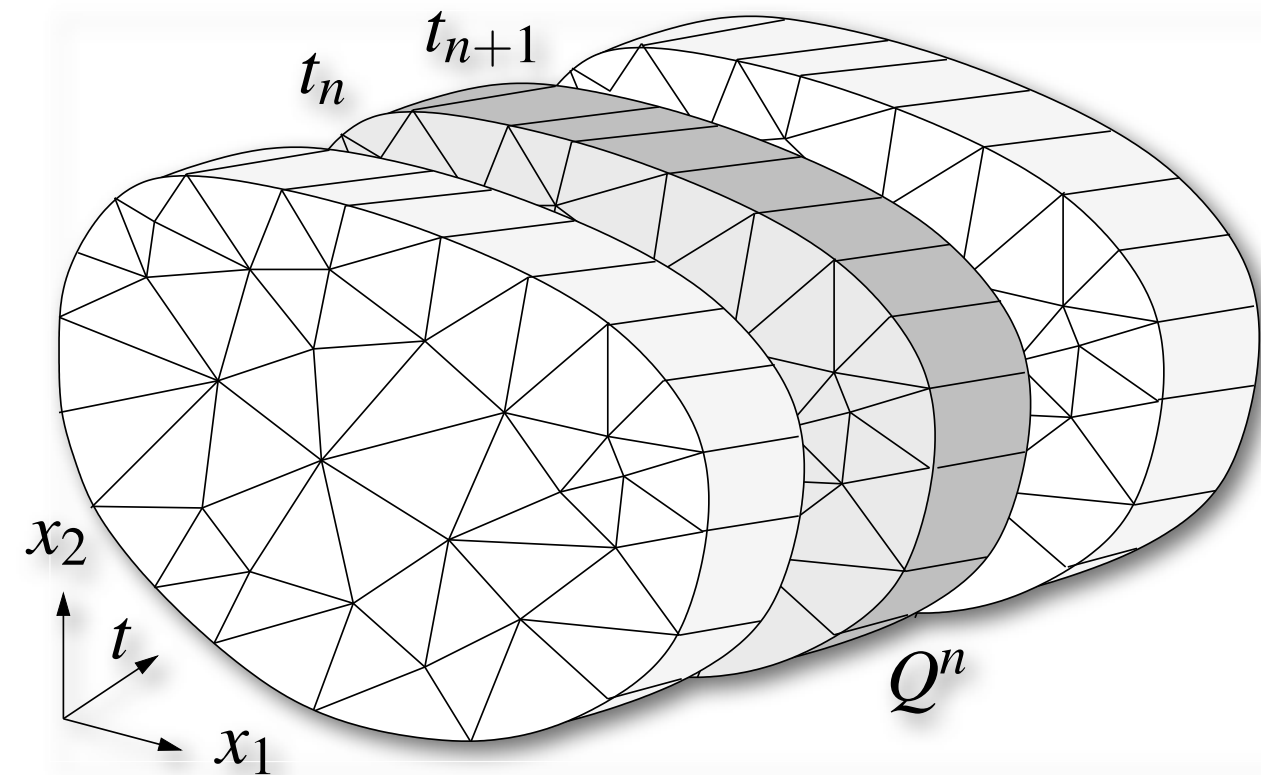
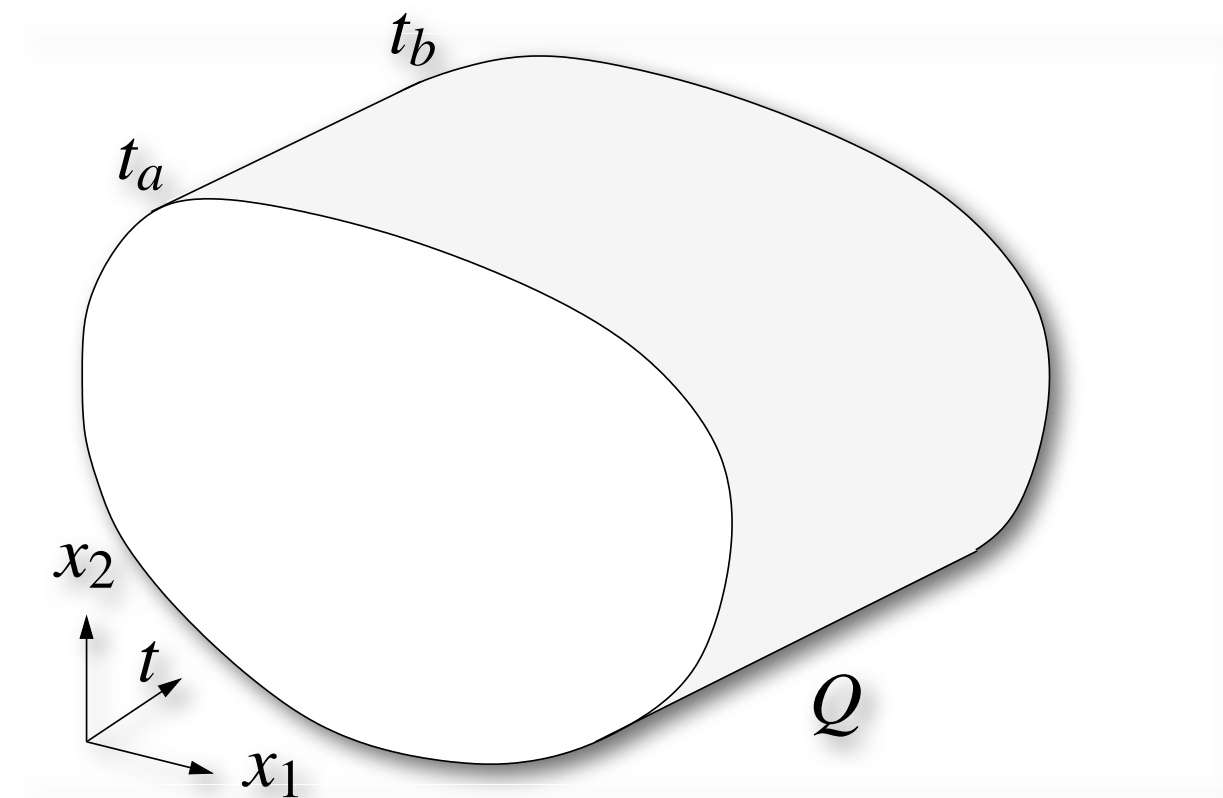
Construction of an updated space-time level set function from the current configuration of the thin structure using

$$\phi(\mathbf{x}, t) = \pm \min_{\mathbf{x} \in \Sigma} (\|\mathbf{x}(t) - \mathbf{x}^\Sigma(t)\|_2)$$



Space-Time Finite Element Approach

- Uniform discretization in space and time using finite elements



- ▶ Straightforward applicability of XFEM technology for evolving non-smooth solution in the space-time domain
- ▶ Enriched space-time finite elements enable the capturing of non-smooth solutions propagating through the domain

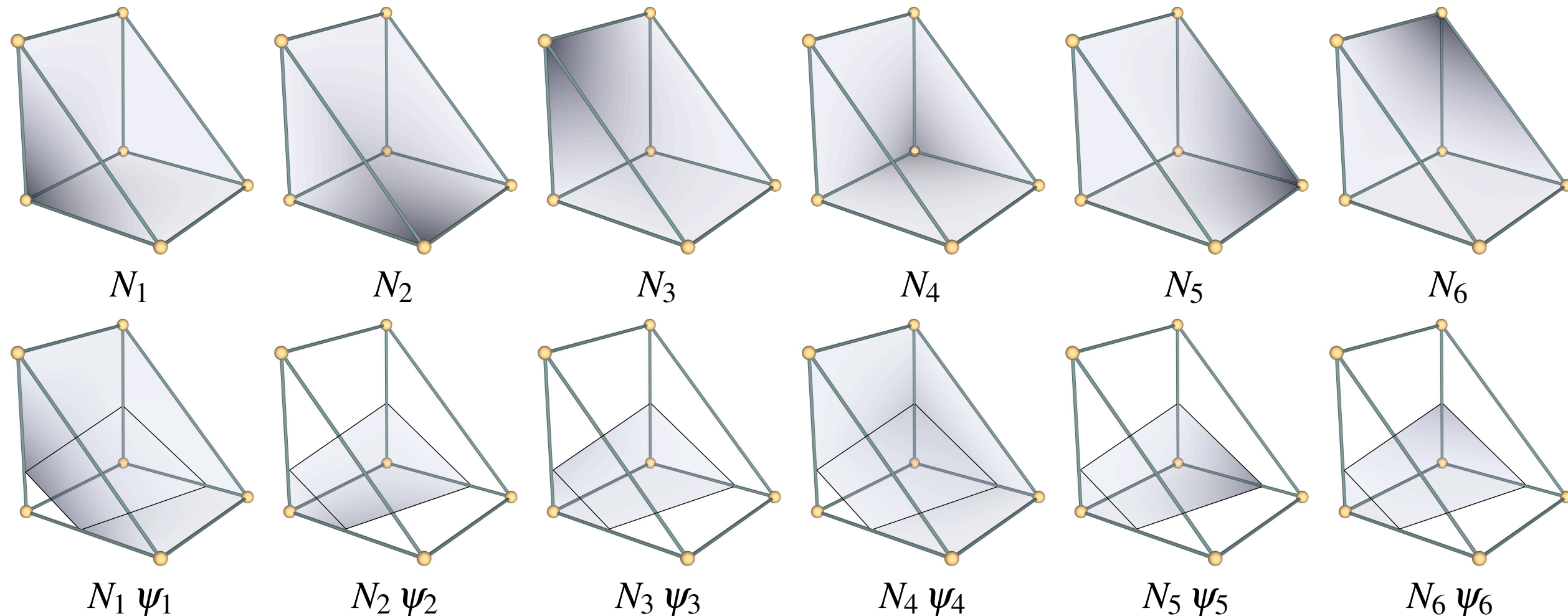
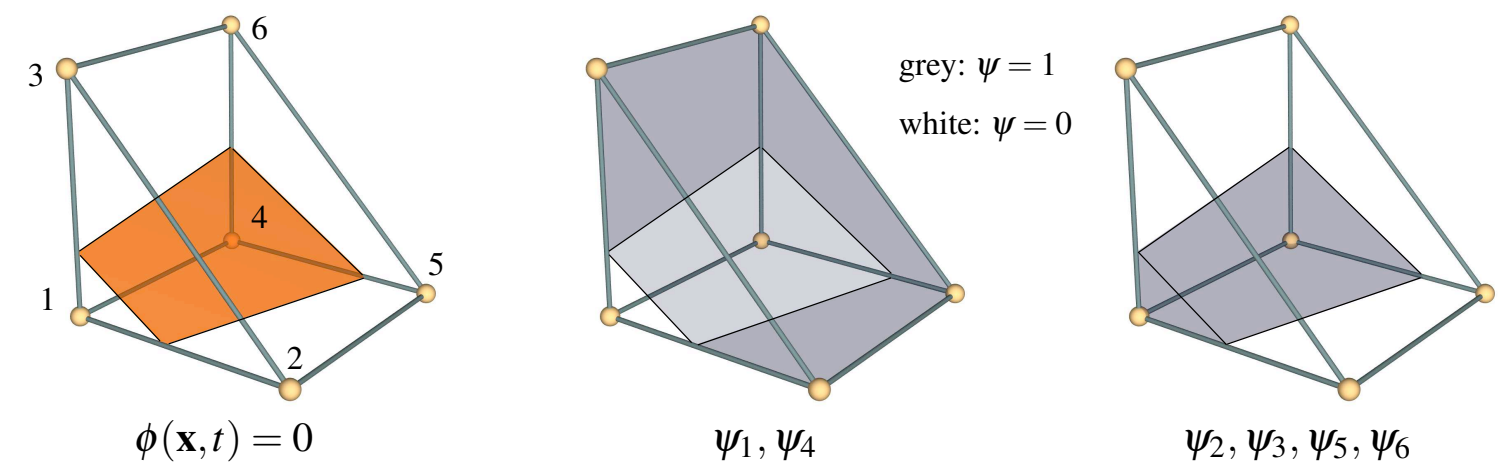
Extrinsic Enrichment of Space-Time FEM

- Combination of level sets, local PUM and space-time finite elements

$$p^F(\mathbf{x}, t) = \sum_{k \in \mathcal{N}} N_k^F(\mathbf{x}, t) p^k + \sum_{j \in \mathcal{M}} N_j^F(\mathbf{x}, t) \psi_j(\mathbf{x}, t) q^j$$

- Enrichment function (jump-type)

$$\psi_j(\mathbf{x}, t) = \frac{1}{2} (1 - \text{sign } \phi(\mathbf{x}, t) \cdot \text{sign } \phi(\mathbf{x}^j, t^j))$$



Enriched Flow Approximation

► Enriched fluid velocity approximation

$$\mathbf{v}^F(\mathbf{x}, t) = \sum_{k \in \mathcal{N}} N_k^F(\mathbf{x}, t) \mathbf{v}^k + \sum_{j \in \mathcal{M}} N_j^F(\mathbf{x}, t) \psi_j(\mathbf{x}, t) \mathbf{w}^j$$

► Enriched Fluid pressure approximation

$$p^F(\mathbf{x}, t) = \sum_{k \in \mathcal{N}} N_k^F(\mathbf{x}, t) p^k + \sum_{j \in \mathcal{M}} N_j^F(\mathbf{x}, t) \psi_j(\mathbf{x}, t) q^j$$

✓ Strong and weak discontinuous flow solutions at immersed structure

➡ Enriched approximation decouples flow state at interface completely!

➡ Impose coupling conditions at fluid-structure interface!

Imposing Interface Conditions

- impose constraints at interface not explicitly discretized (meshed)
- constrained functions are touched by local enrichments (XFEM)
- varying number of involved degrees of freedom (current interface shape)

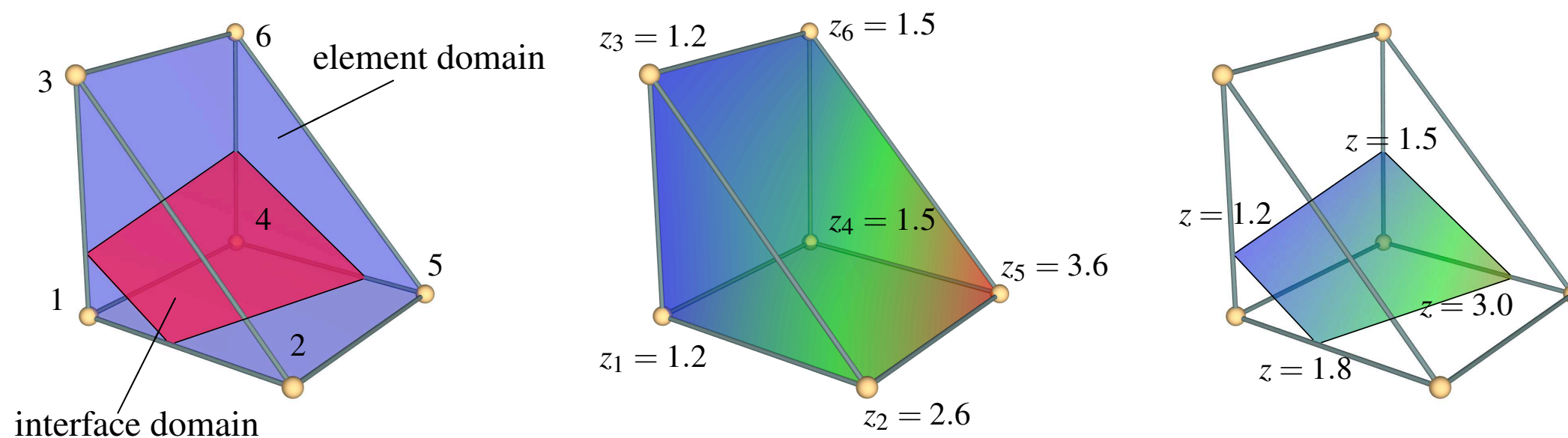
- Penalty methods?
- Lagrangian multiplier?
- Nitsche's method?
- etc.?

Perturbed Lagrangian Multiplier Technique

- implicit formulation of the Lagrange multiplier

$$\mathbf{t}^F = \mathbf{z}^F \delta_D(\phi)$$

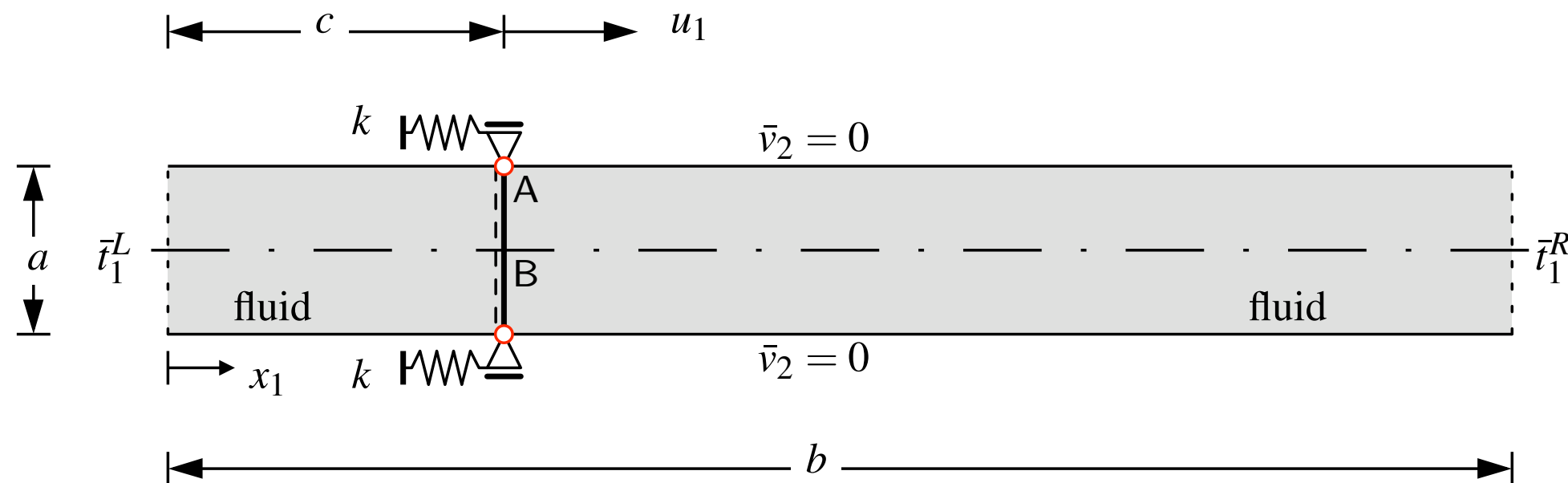
- for constraints at evolving interfaces in combination with Space-Time-FEM



- transformed weak coupling conditions (with perturbation)

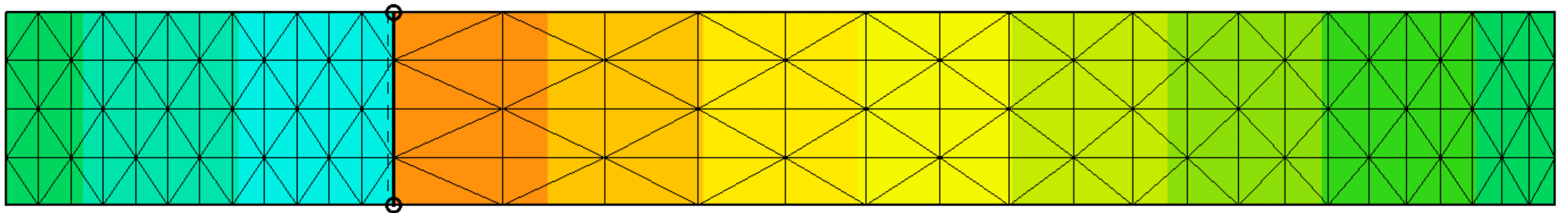
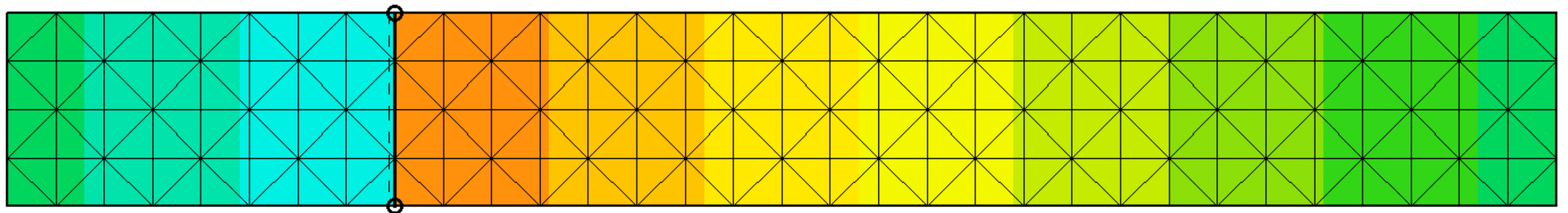
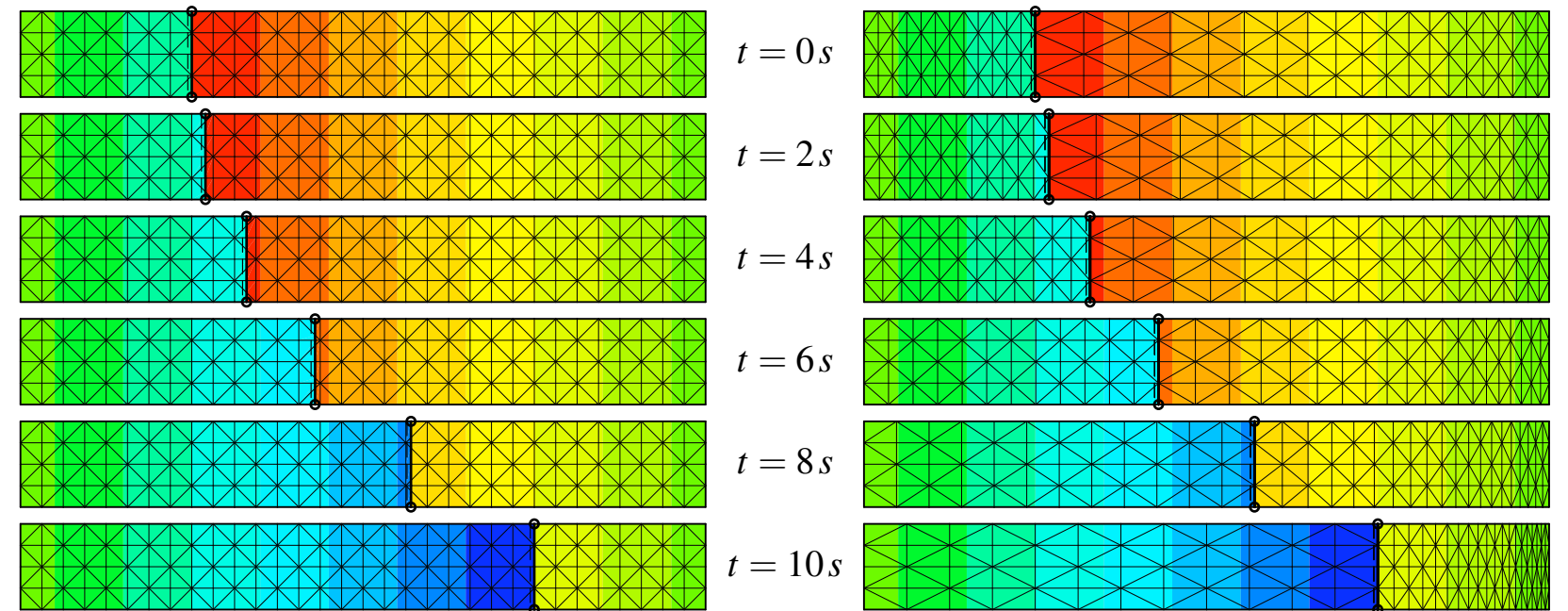
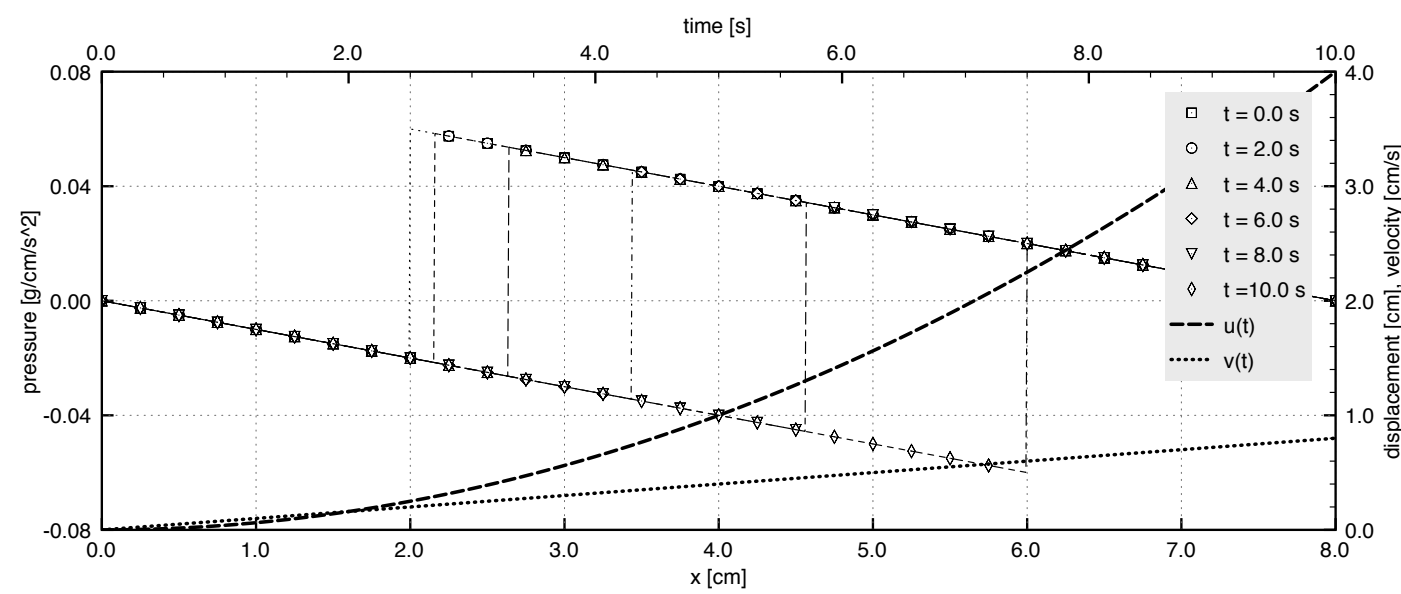
$$\begin{aligned} & + \int_{R_t^{n,+}} \delta \mathbf{z}^{F+} \cdot (\mathbf{v}^{F+} - \mathbf{v}^S) dR - \int_{R_t^{n,+}} \delta \mathbf{v}^{F+} \cdot \mathbf{z}^{F+} dR + \int_{R_t^{n,+}} \delta \mathbf{v}^S \cdot \mathbf{z}^{F+} dR \\ & + \int_{R_t^{n,-}} \delta \mathbf{z}^{F-} \cdot (\mathbf{v}^{F-} - \mathbf{v}^S) dR - \int_{R_t^{n,-}} \delta \mathbf{v}^{F-} \cdot \mathbf{z}^{F-} dR + \int_{R_t^{n,-}} \delta \mathbf{v}^S \cdot \mathbf{z}^{F-} dR \\ & + \sum_{e \in \mathcal{Z}} \int_{Q_t^{n,e}} \delta \mathbf{z}^{F+} \cdot \boldsymbol{\tau}_z \mathbf{z}^{F+} + \sum_{e \in \mathcal{Z}} \int_{Q_t^{n,e}} \delta \mathbf{z}^{F-} \cdot \boldsymbol{\tau}_z \mathbf{z}^{F-}, \end{aligned}$$

Example: Piston I - Problem Setup

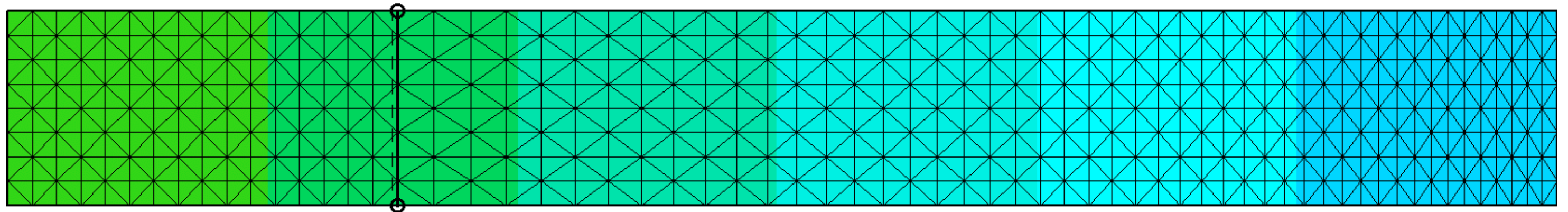
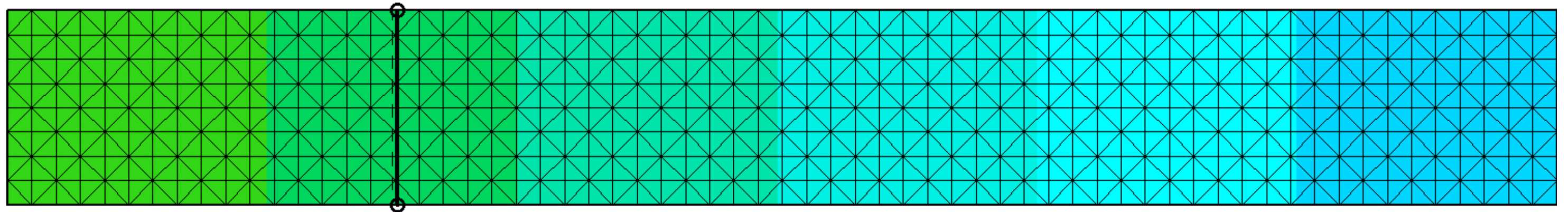
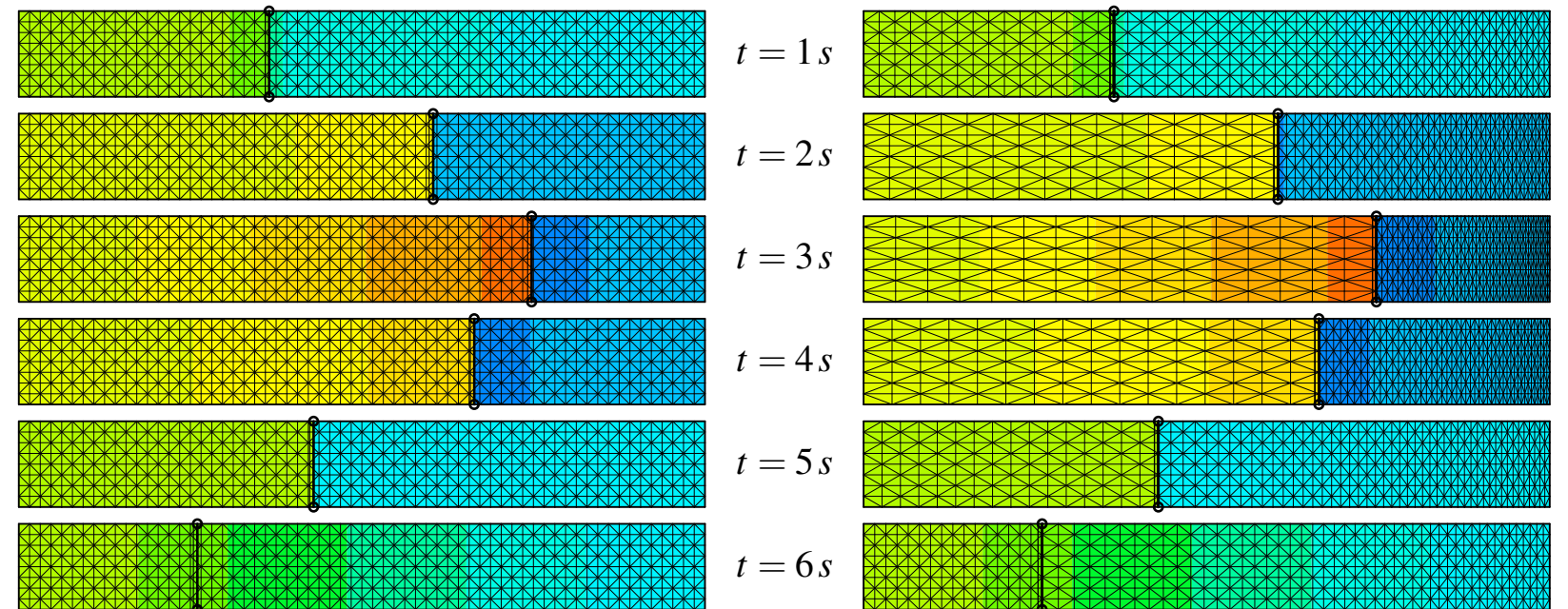
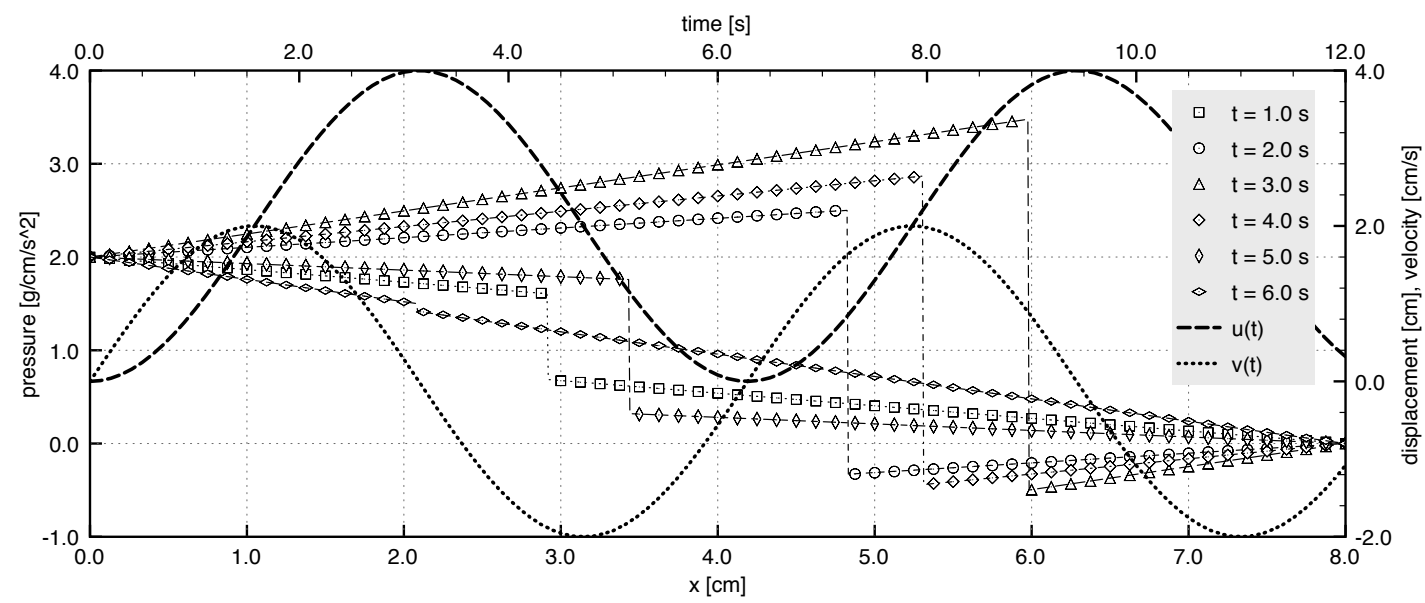


$$p(x_1, t) = \begin{cases} \bar{t}_1^L - \rho_f v_{1,t}^A(t) x_1 & x_1 < X^A(t) \\ \bar{t}_1^R + \rho_f v_{1,t}^A(t) (b - x_1) & x_1 > X^A(t) \end{cases}$$

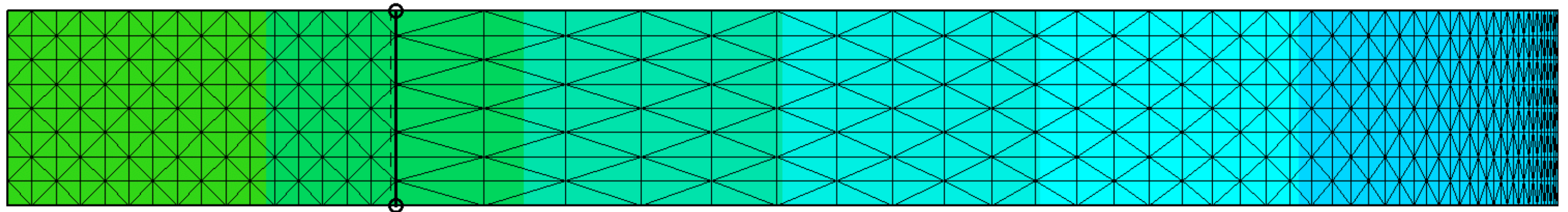
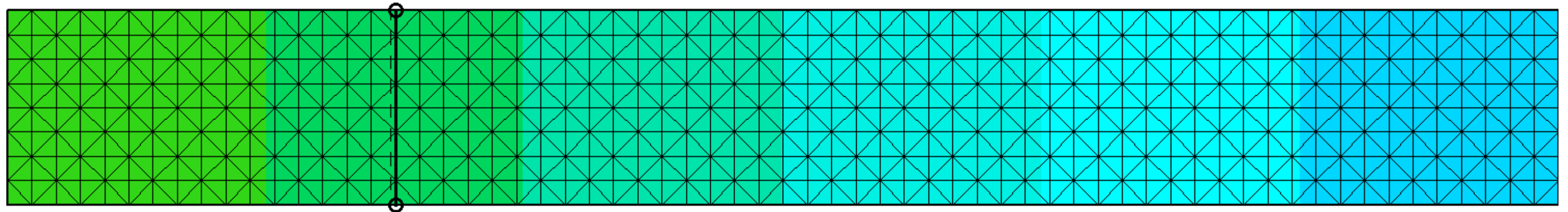
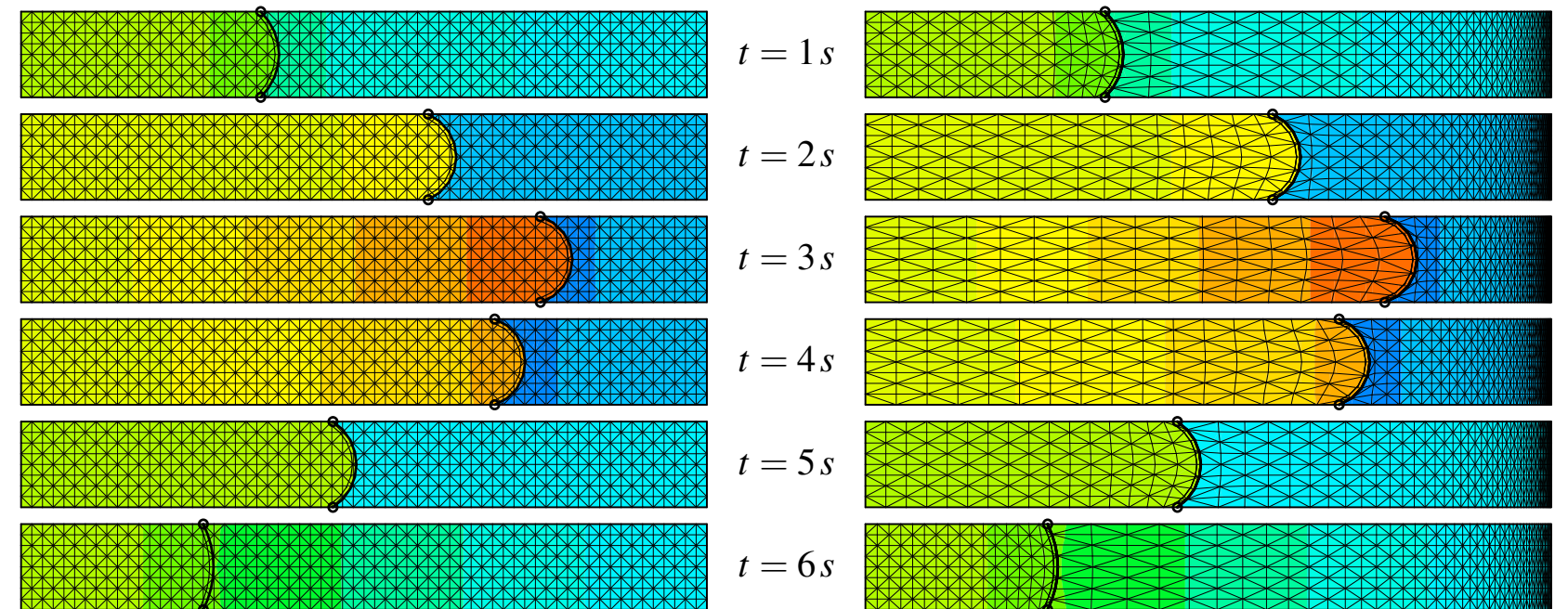
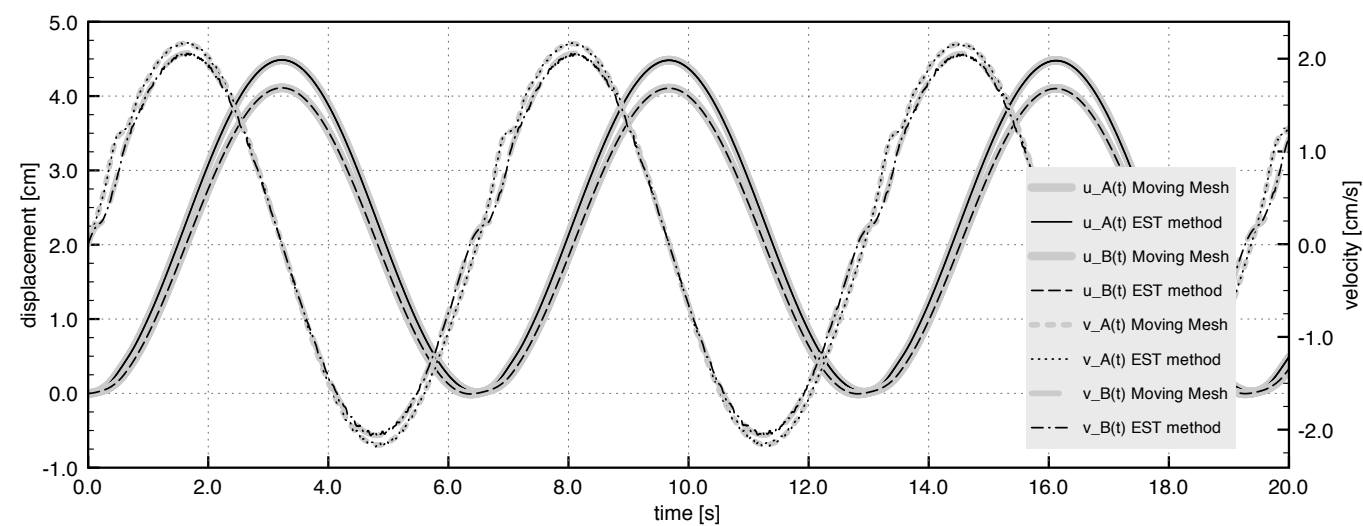
Example: Piston II - Prescribed Motion



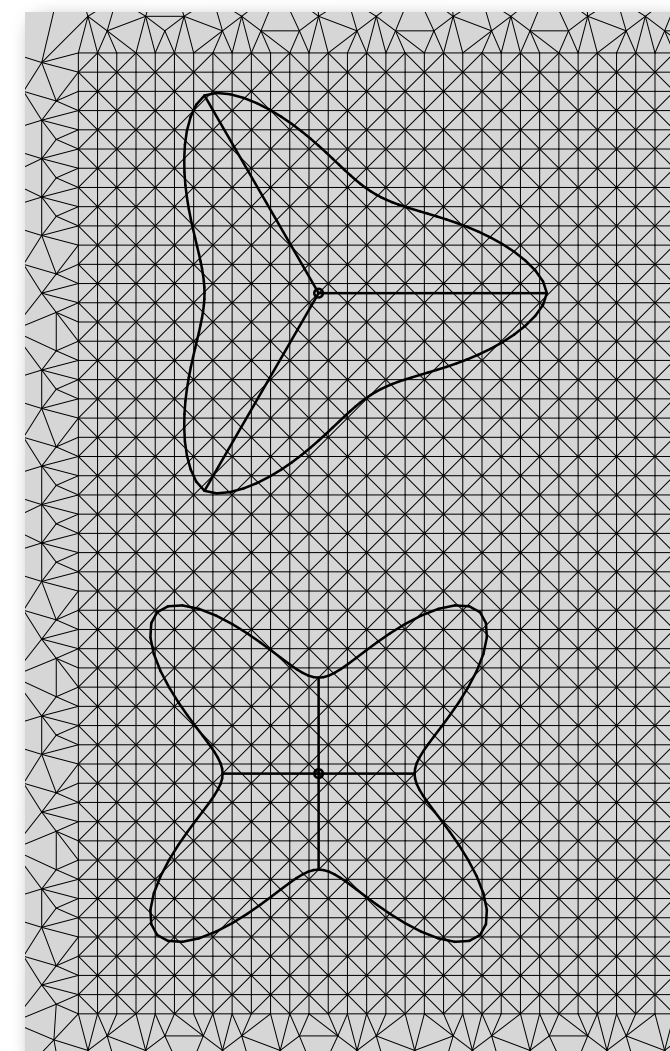
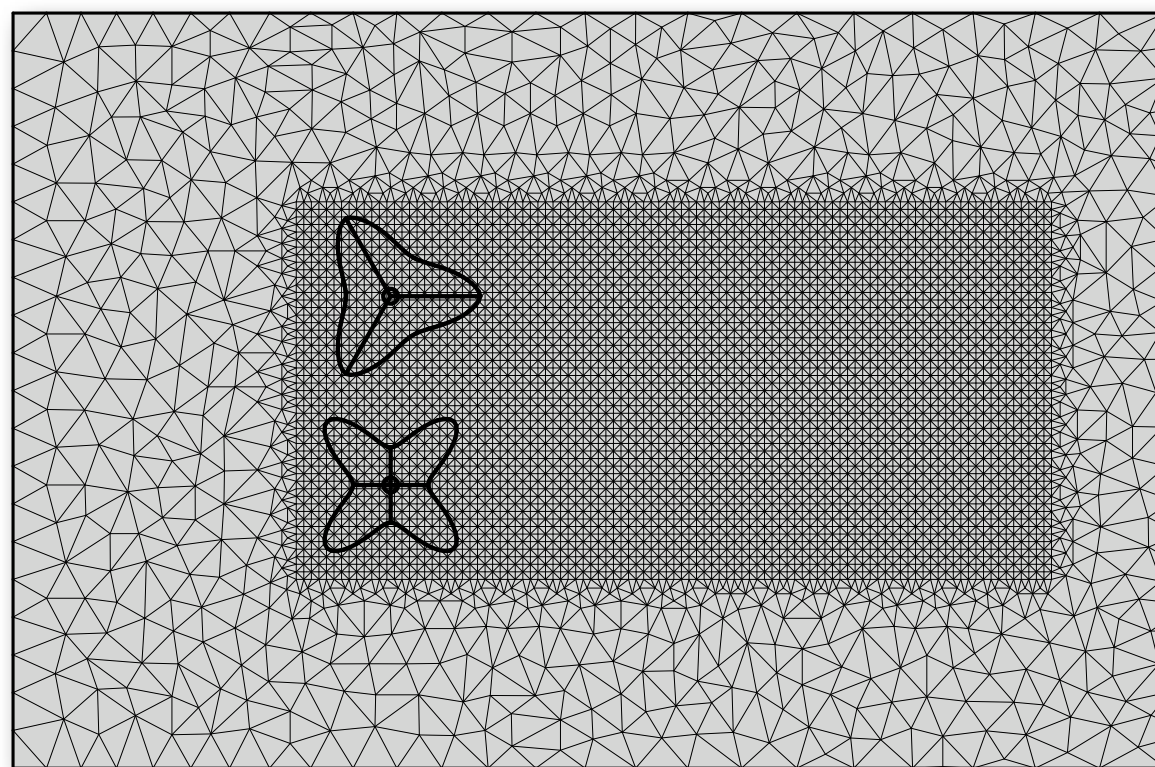
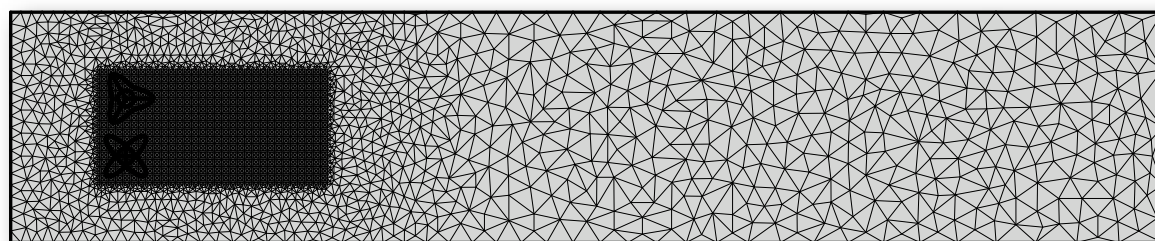
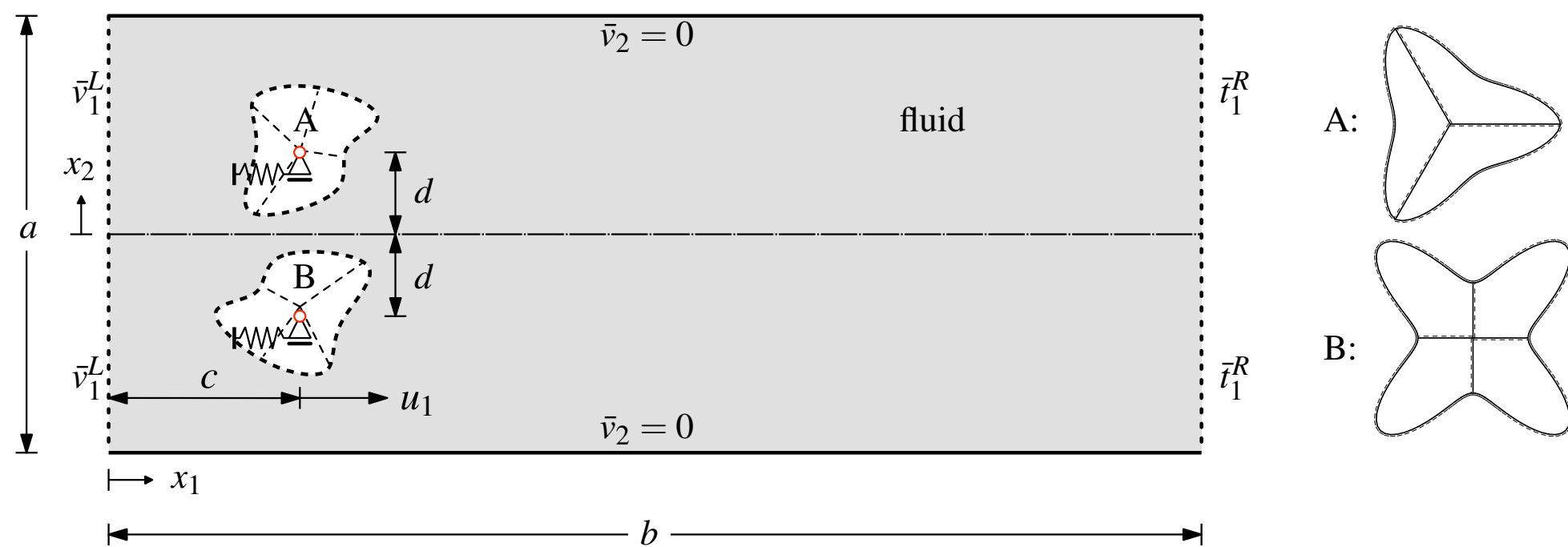
Example: Piston II - Rigid with Spring



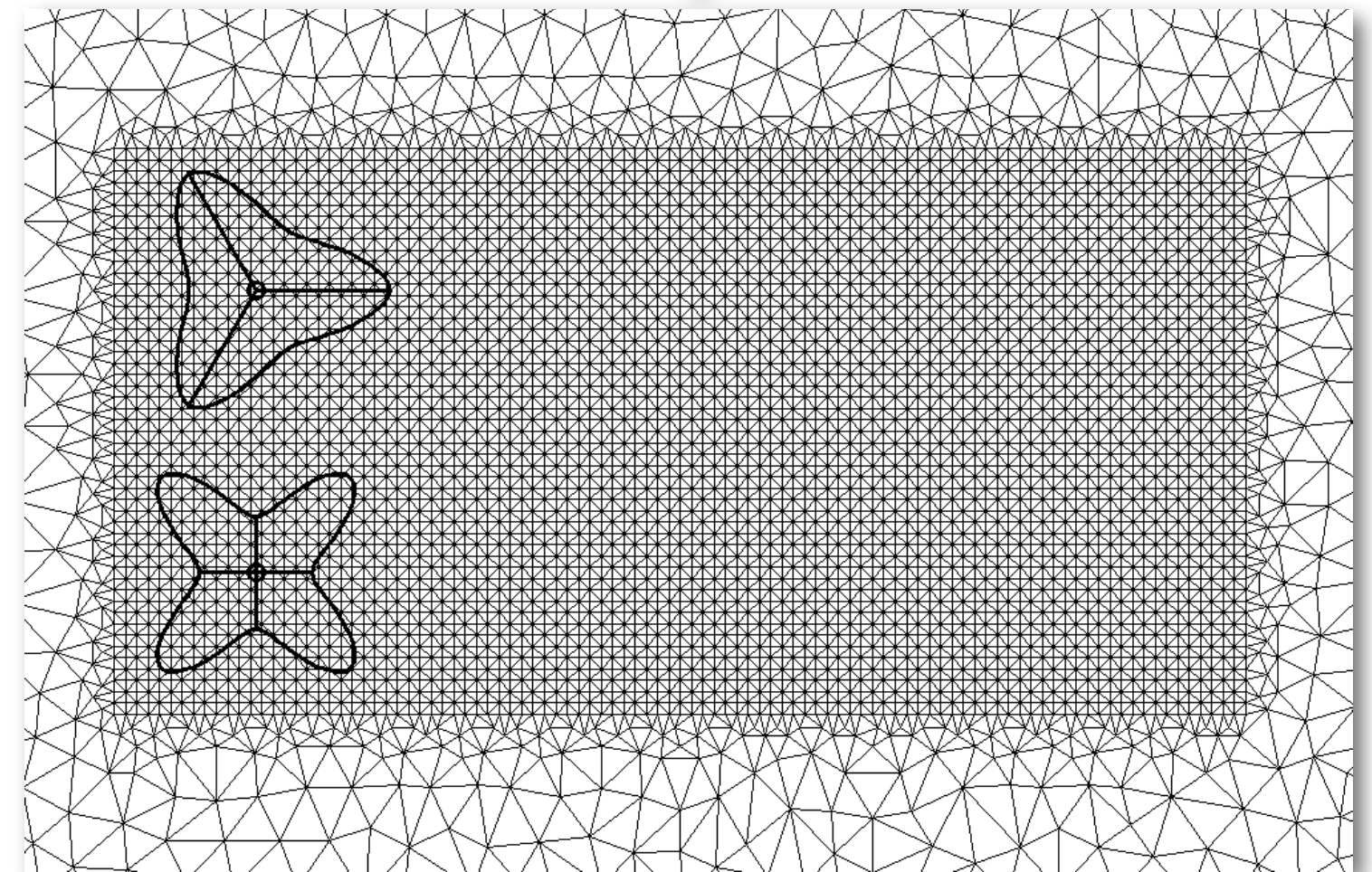
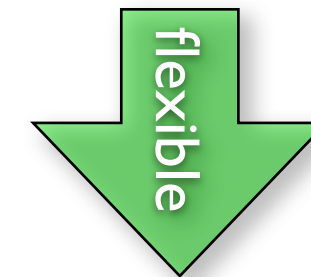
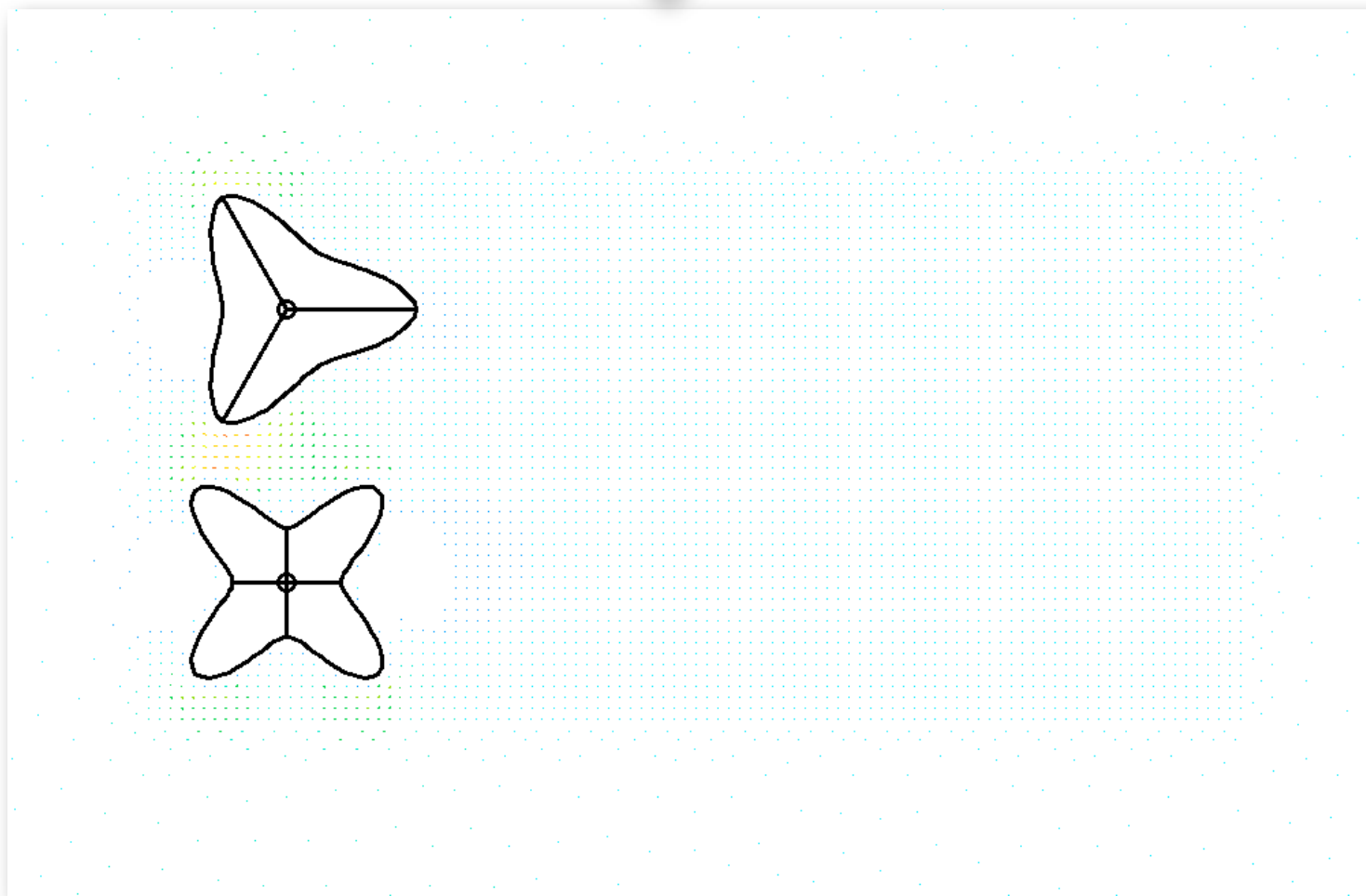
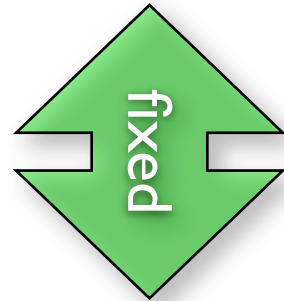
Example: Piston III - Flexible with Spring



Example: Multiple Rotating Structures I



Example: Multiple Rotating Structures II



Contact

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